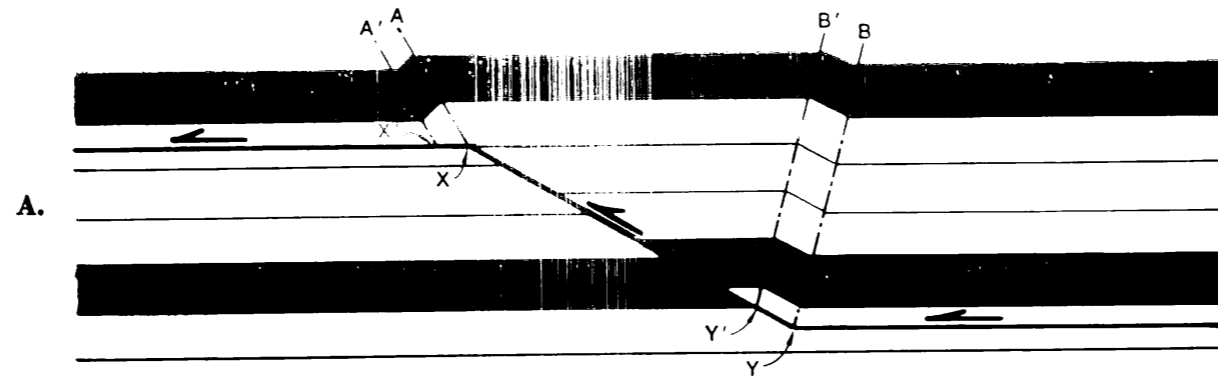
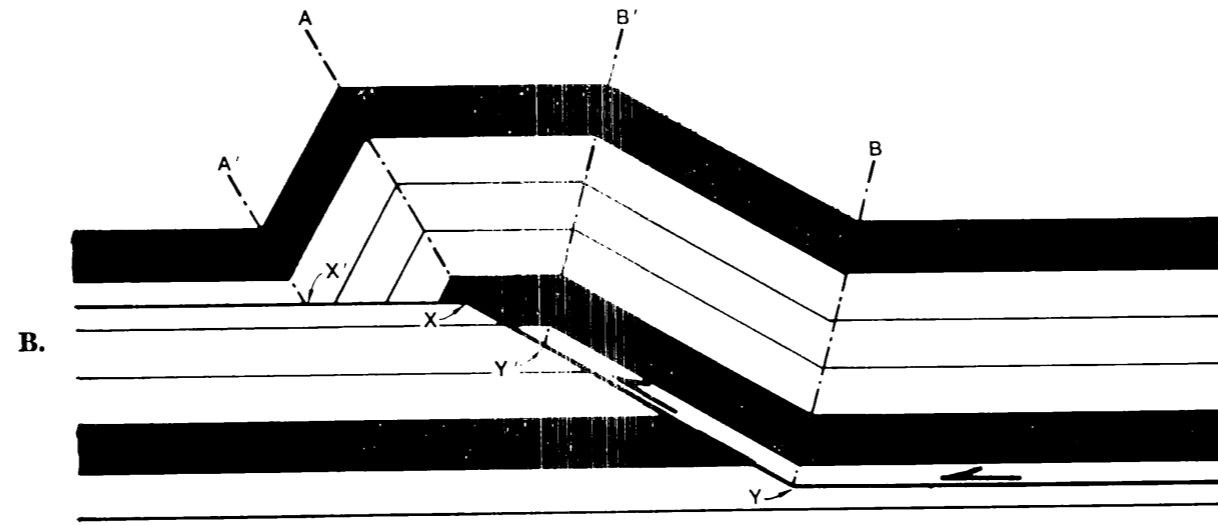


# Fault-bend fold



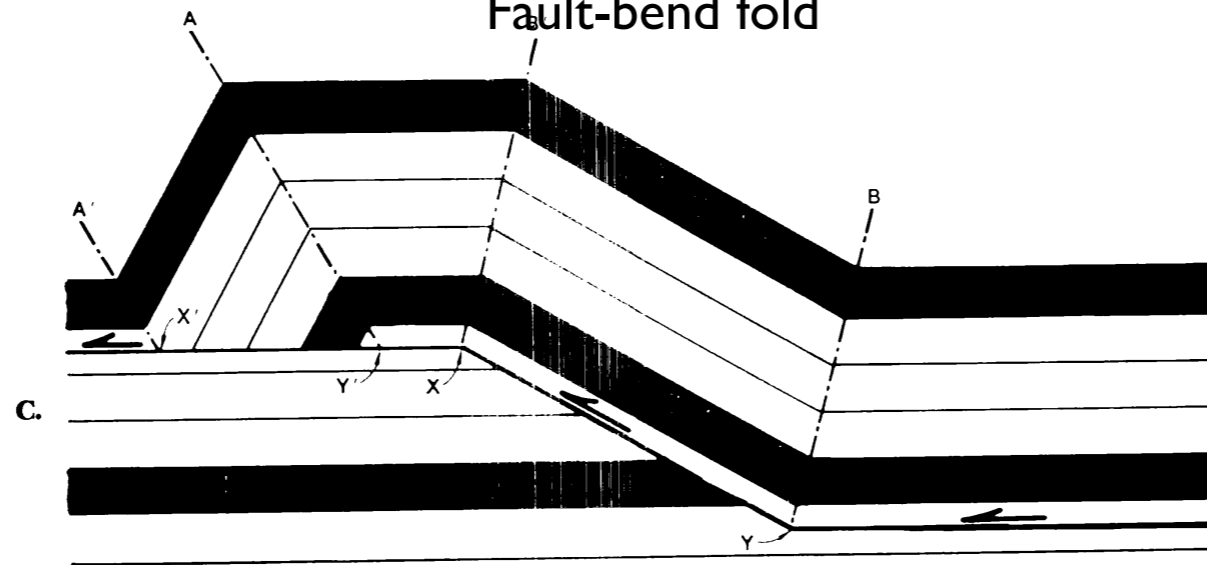
Suppe, 1983

# Fault-bend fold



Suppe, 1983

## Fault-bend fold



### Advantages:

Can be reconstructed from surface geology

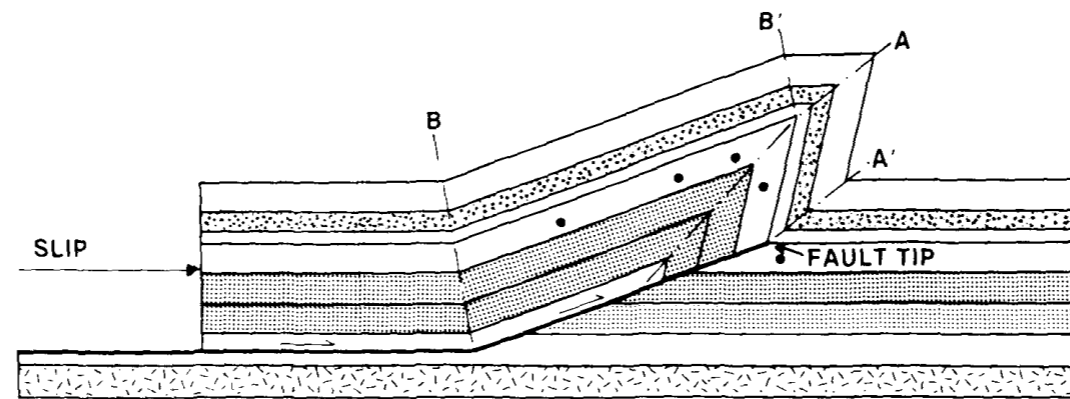
### Assumptions:

Pervasive slip on bedding planes as rocks pass through hinges

Slip is carried off-section (no deformation of lower plate)

Suppe, 1983

# Fault-Propagation fold



Namson and Davis, GSA Bull , 1988 after Suppe and Medwedeff, 1984



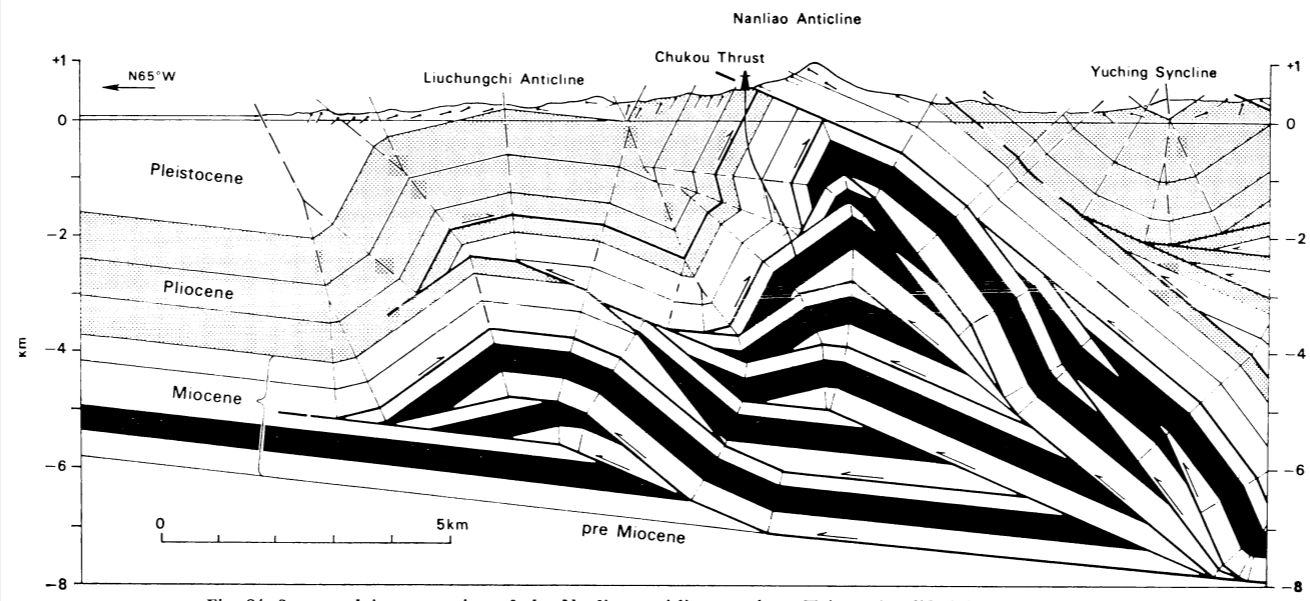
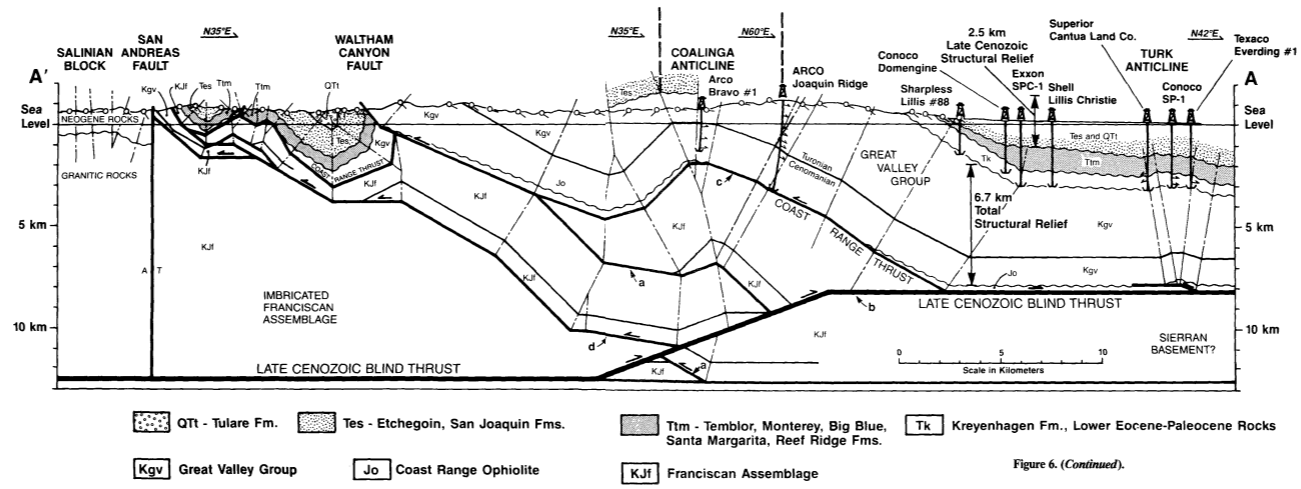


Fig. 24. Structural interpretation of the Nanliao anticline, southern Taiwan (modified from Suppe, 1980b).

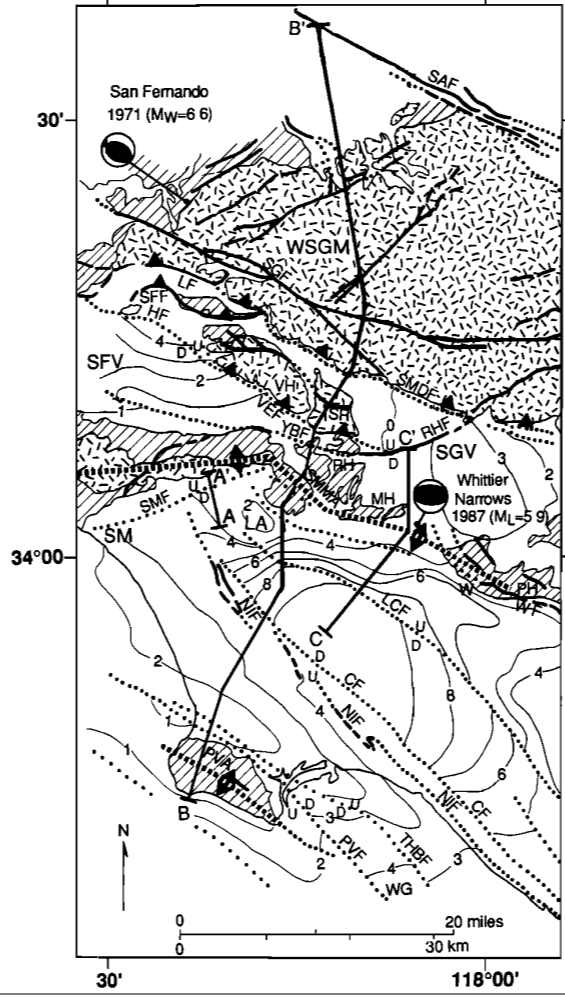
Suppe, 1983

# Coalinga, California (site of 1983 earthquake)

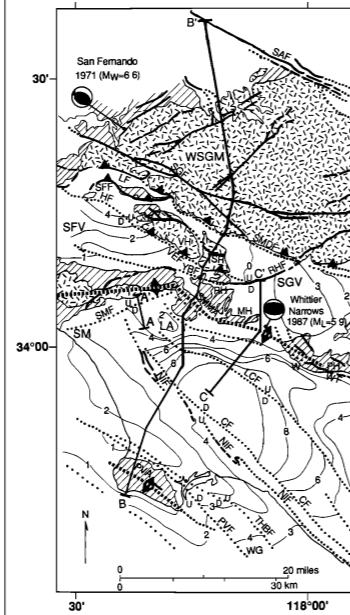
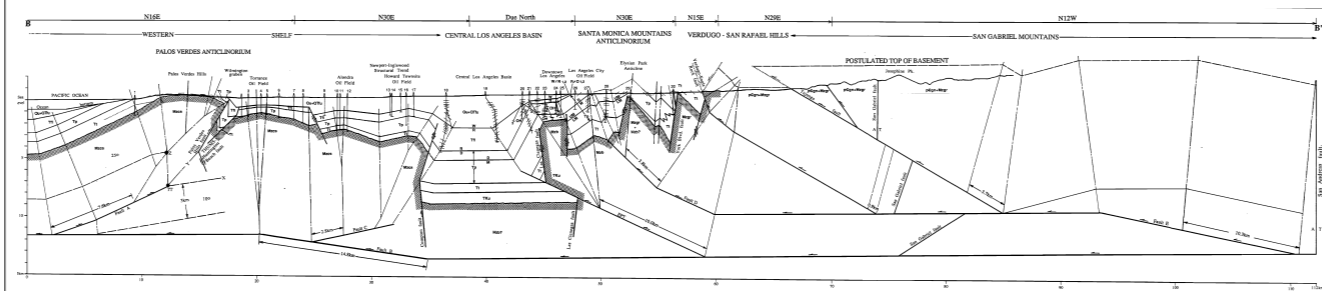


Namson and Davis, GSA Bull , 1988

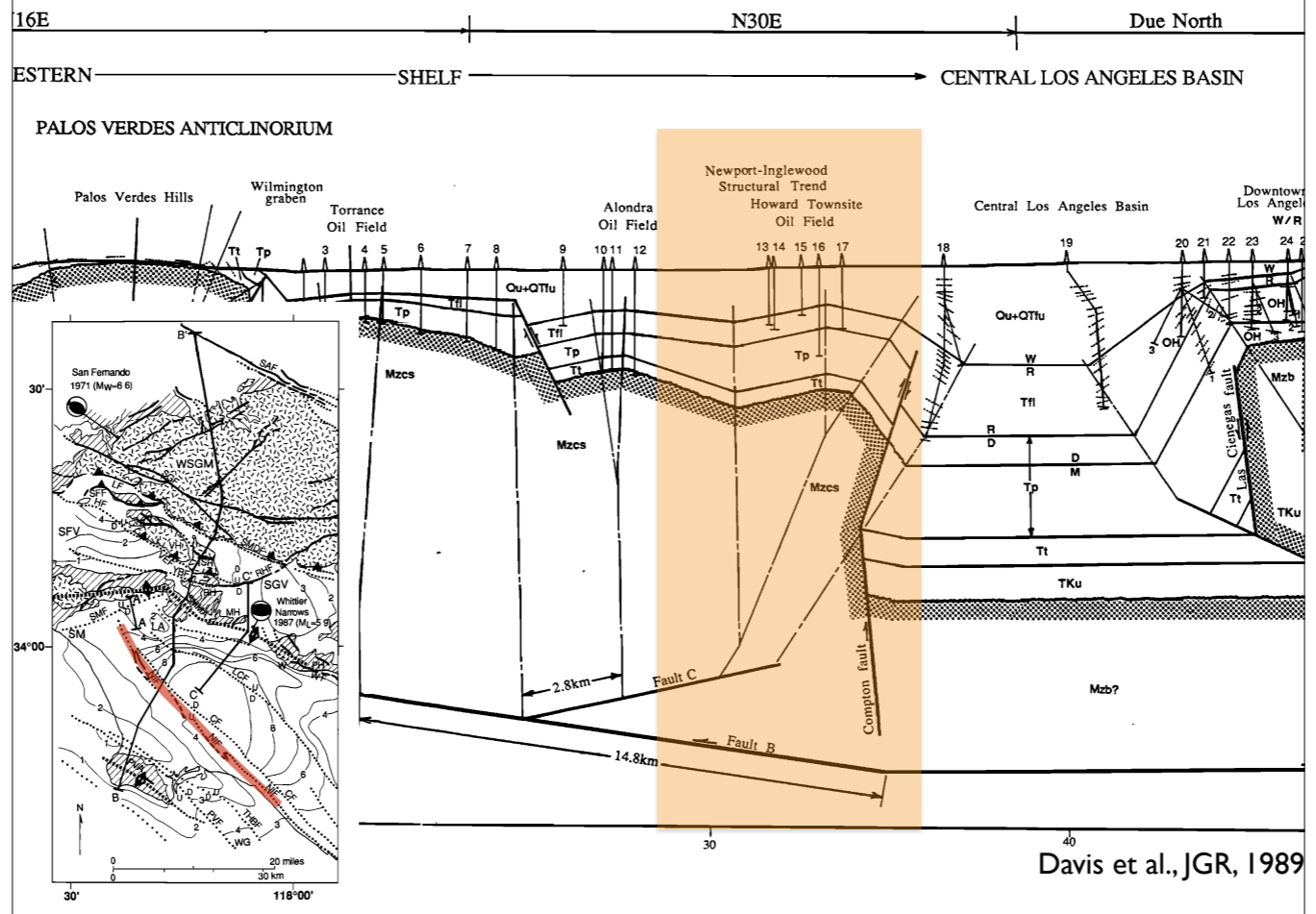
Coalinga anticline grew in the earthquake, which lacked any surface faulting.

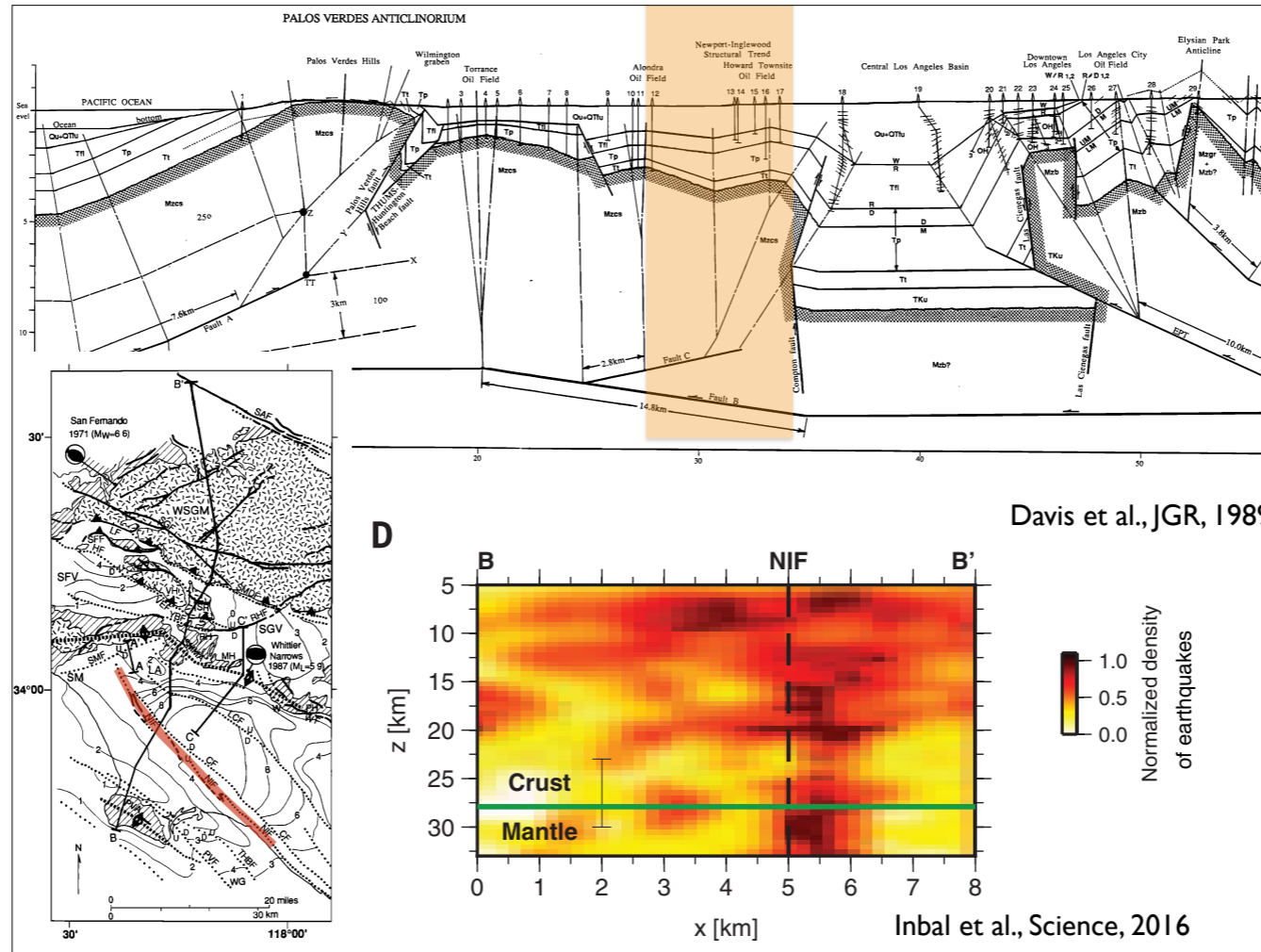


Davis et al., JGR, 1989



Davis et al., JGR, 1989





Inbal et al. got lots of small EQs from a very dense array and see the Newport-Inglewood fault extending into the mantle, not detached as thought by Davis et al. This helps reveal a weakness of the geometric reconstructions of fold belts: they need detachment to go off the edge of the model at the side.

## FORELAND STRUCTURAL MODELS

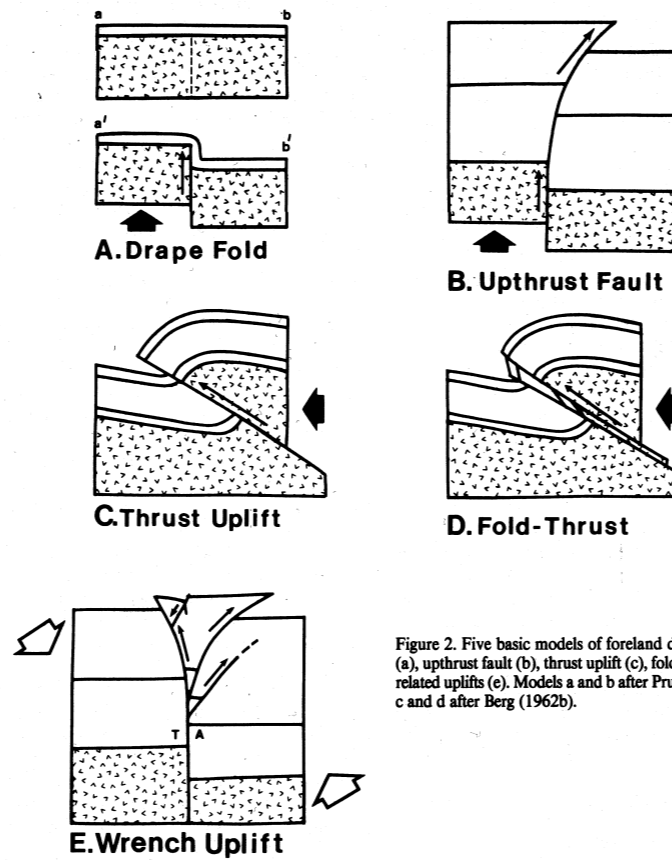


Figure 2. Five basic models of foreland deformation are the drape fold (a), upthrust fault (b), thrust uplift (c), fold-thrust uplift (d), and wrench-related uplifts (e). Models a and b after Prucha and others (1965); models c and d after Berg (1962b).

Brown, GSA Mem 171, 1988

Well, as a prelude to the Laramide, let's discuss a different flavor of this: basement cored folds.

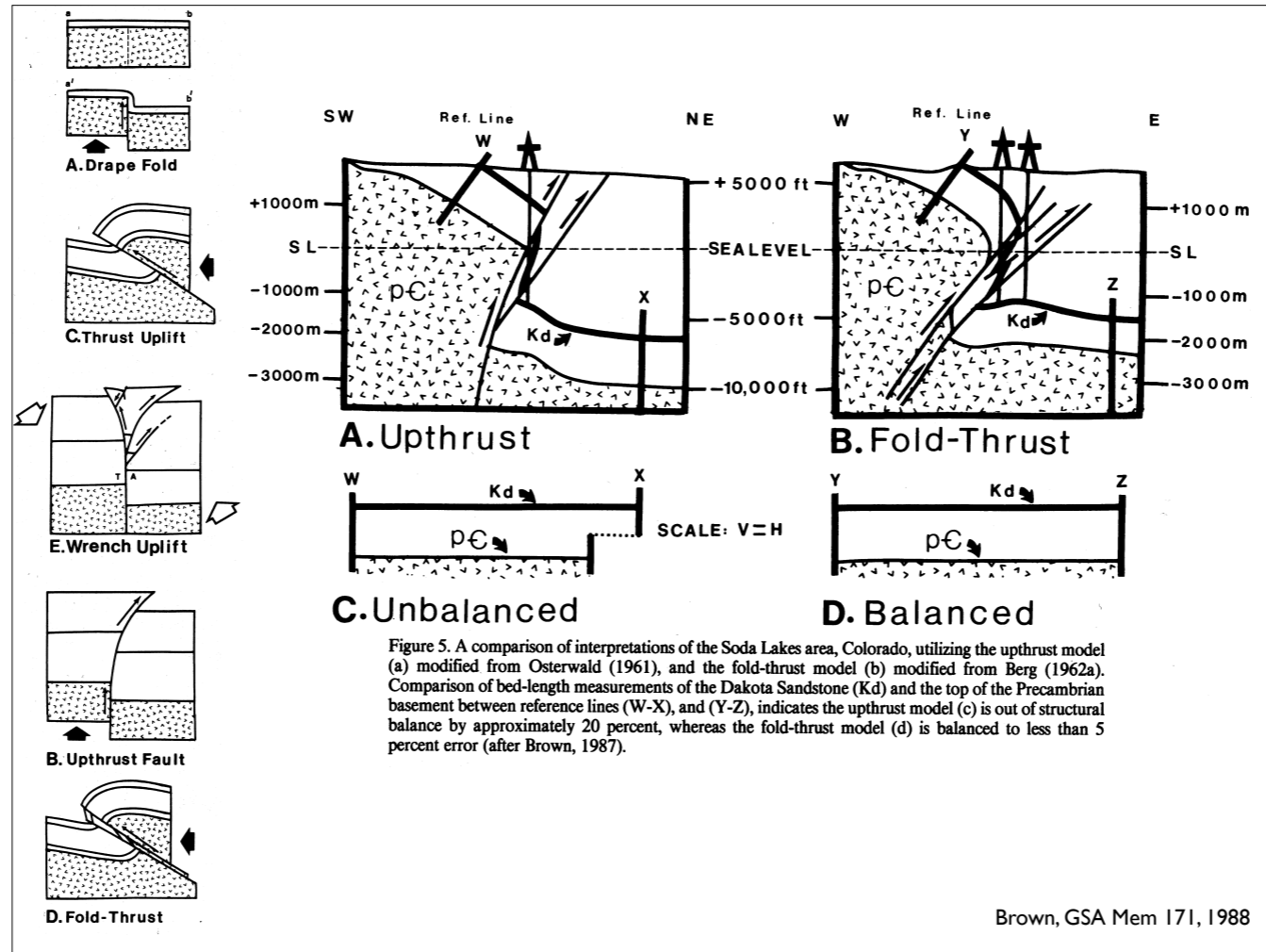
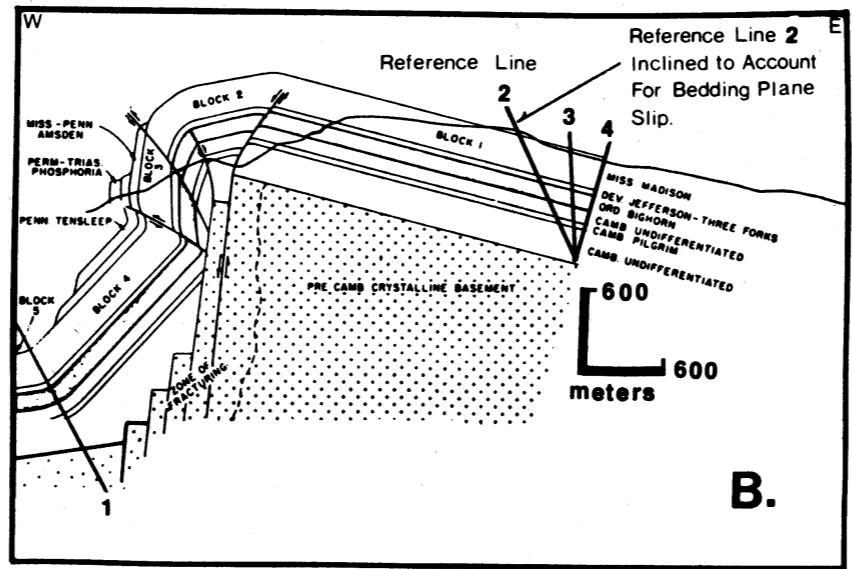
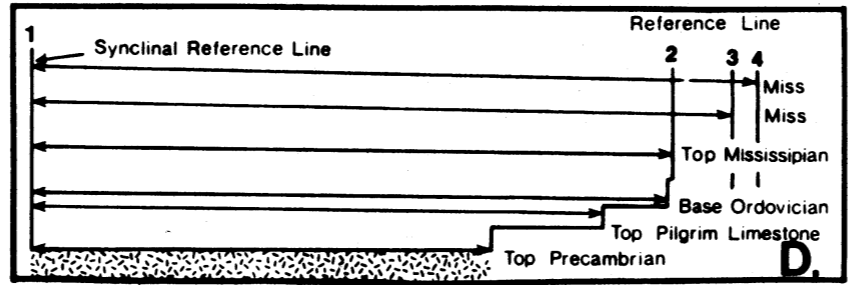


Figure 5. A comparison of interpretations of the Soda Lakes area, Colorado, utilizing the upthrust model (a) modified from Osterwald (1961), and the fold-thrust model (b) modified from Berg (1962a). Comparison of bed-length measurements of the Dakota Sandstone (Kd) and the top of the Precambrian basement between reference lines (W-X), and (Y-Z), indicates the upthrust model (c) is out of structural balance by approximately 20 percent, whereas the fold-thrust model (d) is balanced to less than 5 percent error (after Brown, 1987).

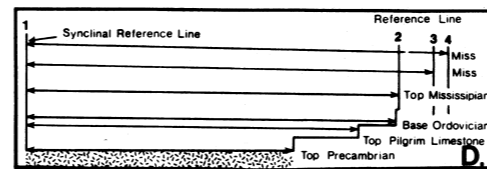
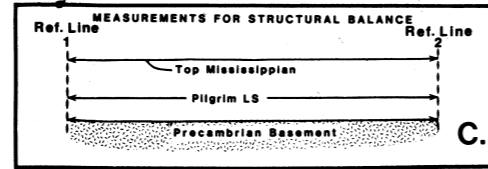
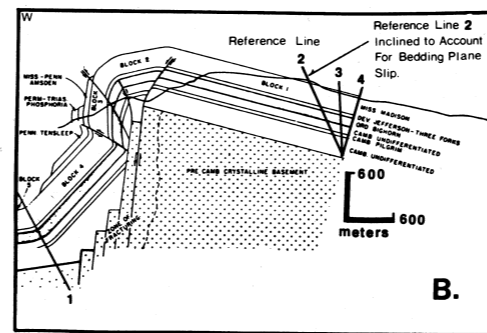
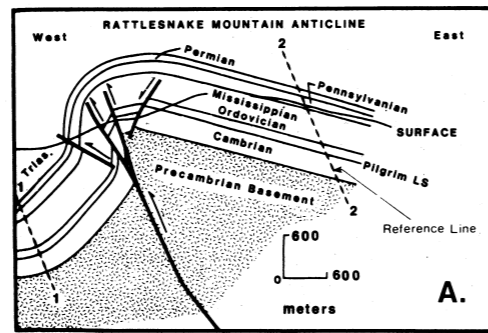




Rattlesnake Mtn  
interpretation of  
Sterns, 1971



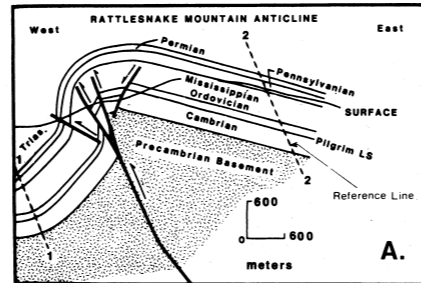
Brown, GSA Mem 171, 1988



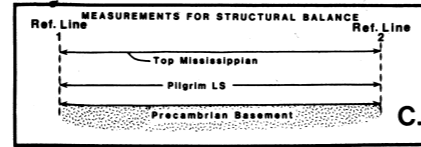
Rattlesnake Mtn  
interpretation of  
Brown, 1984

Rattlesnake Mtn  
interpretation of  
Sterns, 1971

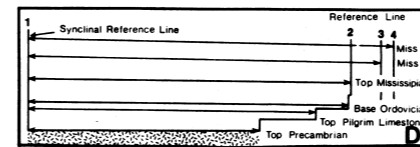
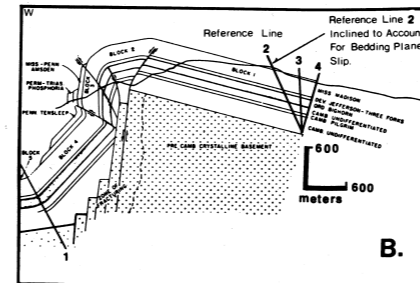
Rattlesnake Mtn interpretation of Brown, 1984



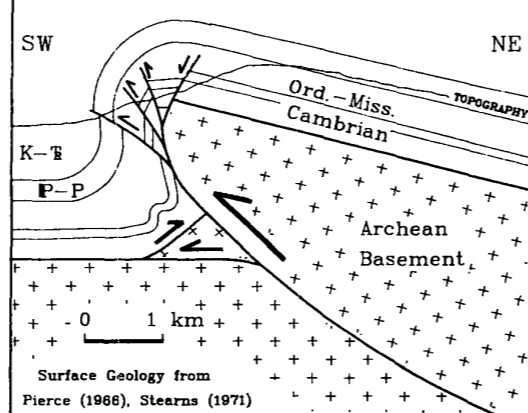
Rattlesnake Mtn interpretation of Erslev, 1986



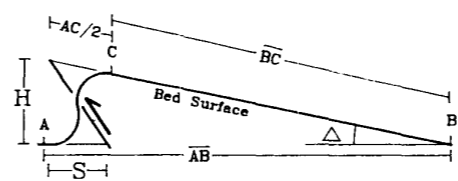
Rattlesnake Mtn interpretation of Sterns, 1971



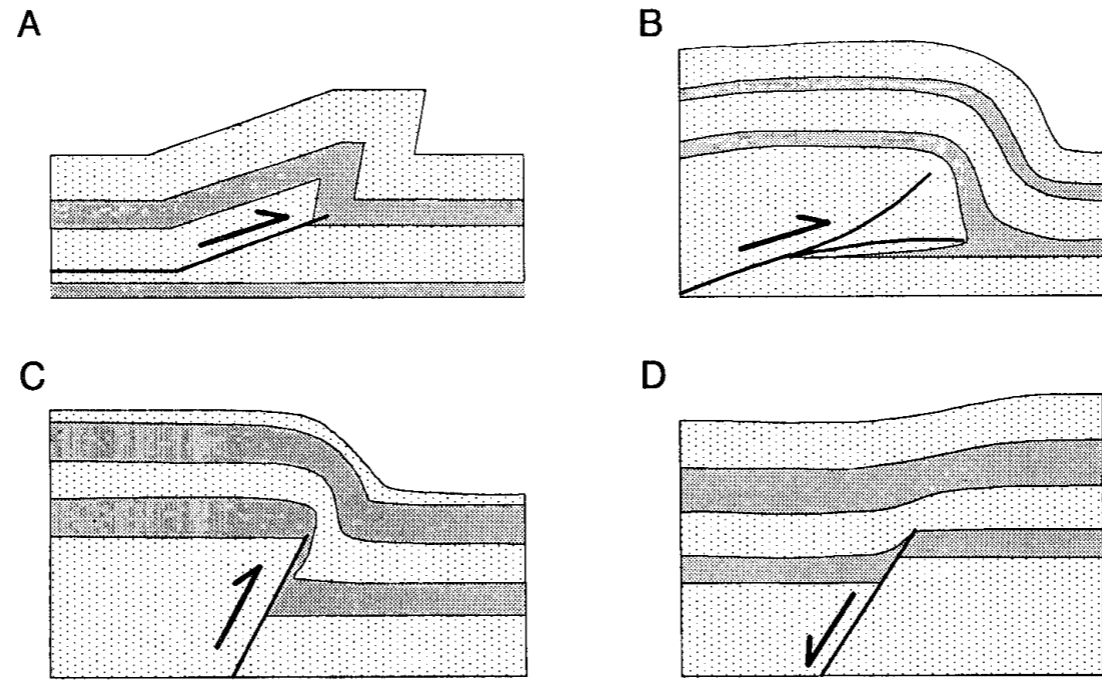
A. Rattlesnake Mtn., Wyoming



B. Fault Dip Calculation

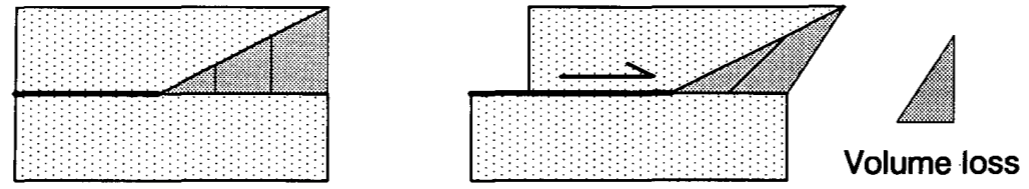


$\Delta$  = Hanging Wall Dip - Footwall Dip  
 AC and AB are Bed Lengths  
 $H = (\overline{BC} + AC/2) \sin \Delta$   
 $S = \text{Total Shortening} - \text{Tilt Shortening}$   
 $S = AB - \overline{AB} - (\overline{BC} + AC/2) (1 - \cos \Delta)$   
 Fault Dip Relative to Footwall =  $\arctan (H/S)$

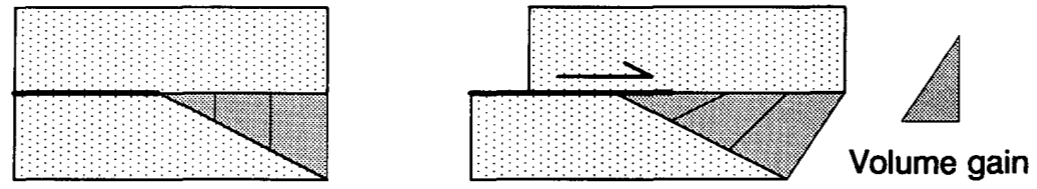


**Figure 1. Models of fault-propagation folds. A: Geometric kink-band model (Suppe and Medwedeff, 1984). B, C, D: Analog experimental models of folds above thrust (B; Chester et al., 1988), reverse (C; Friedman et al., 1980), and normal (D; Withjack et al., 1990) faults.**

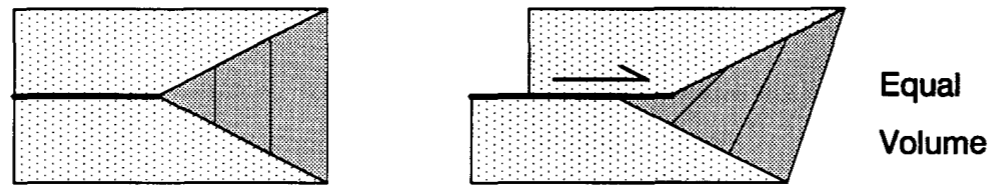
**A. Hanging-Wall Triangular Shear Zone**



**B. Footwall Triangular Shear Zone**



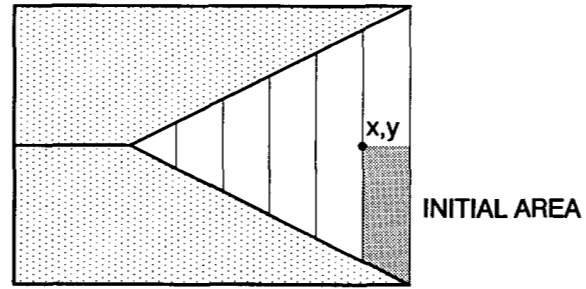
**C. Symmetric Triangular Shear Zone**



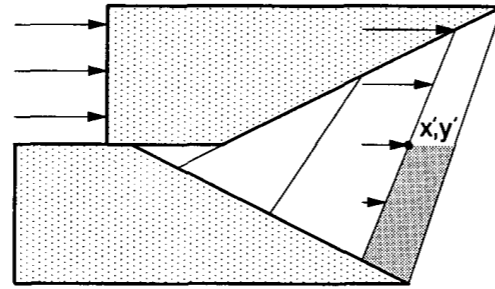
**Figure 2. Geometric end members of triangular shear-zone folding.**

Erslev, 1991

### A. Initial Geometry

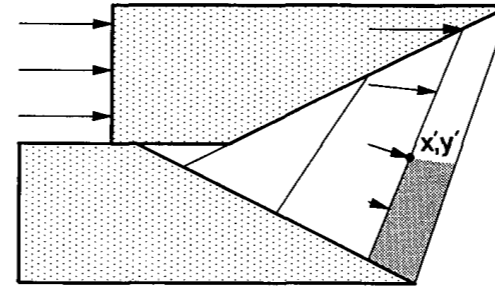


### B. Simple Shear



DEFORMED AREA > INITIAL AREA

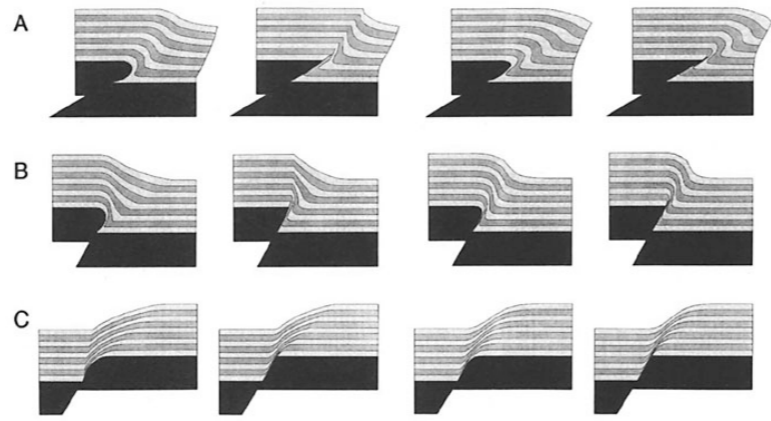
### C. Trishear



DEFORMED AREA = INITIAL AREA

**Figure 3. Simple shear and trishear approximations of homogeneous shear in triangular shear zones.**

Erslev, 1991



**Advantages:**  
 Deals with more realistic geometries in foreland situations than fault-bend folds

**Disadvantages:**  
 Requires plastic deformation in trishear zone, which can become non-unique in terms of structures

Figure 4. TRISHEAR-generated, homogeneous and heterogeneous fault-propagation folding above (A) thrust (30° dip, 60° apex angle), (B) reverse (60° dip, 60° apex angle), and (C) normal (60° dip, 40° apex angle) faults.

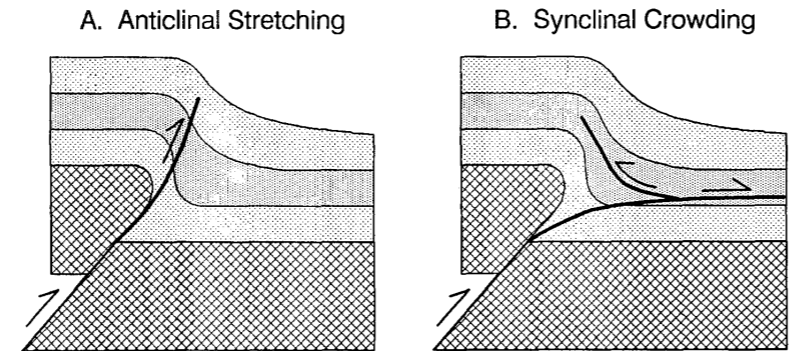


Figure 5. Fault-propagation trajectories suggested by homogeneous, footwall-fixed trishear in front of thrust faults (45° dip, 60° apex angle).

Erslev, 1991

POSTULATED ATTITUDES OF WIND RIVER THRUST

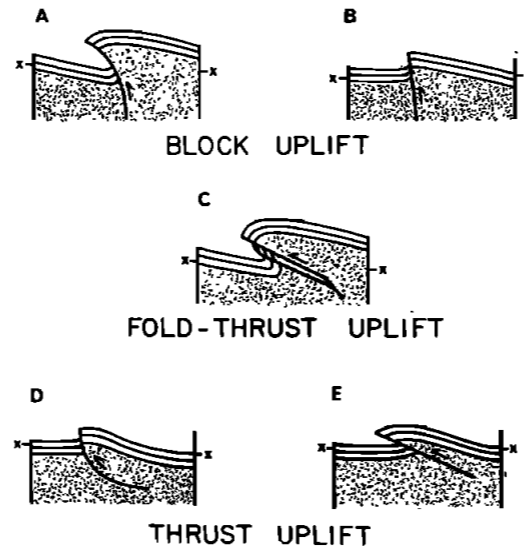


Fig. 1. Proposed structural styles for the Wind River fault. Structure between that in Figure 1c and in 1e is representative of the fault at depth; x-x represents the position of the present ground surface.



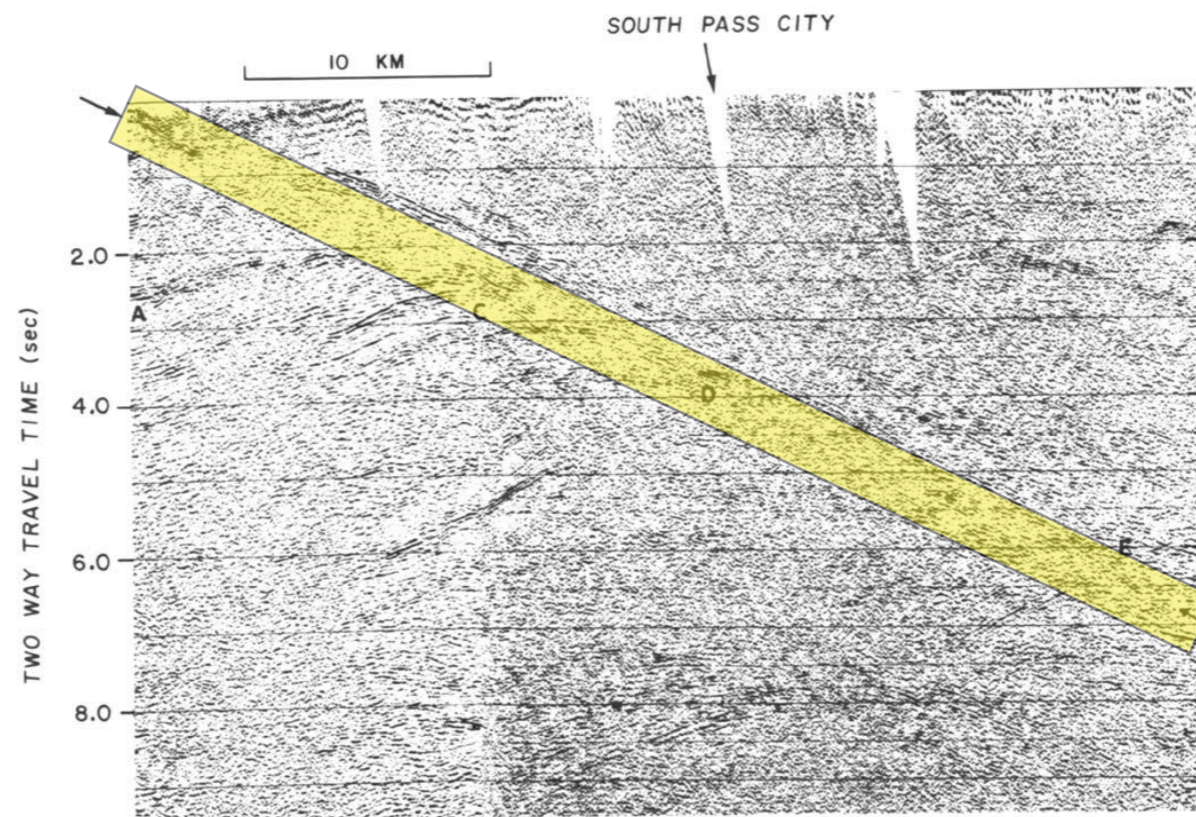


Figure 3. Unmigrated 24-fold CDP stacked reflection profile representing the upper portion of the Wind River thrust. Arrows define the position of the events representing reflections from the thrust plane. A = reflections from flat-lying sediments of Green River Basin. C = uplift (in line sections) of sedimentary reflectors under fault with no evidence of overturning. D = position of thrust against base of sediments. E = thrust reflection in the Precambrian crystalline rocks of the crust. Smithson et al., Geology, 1978

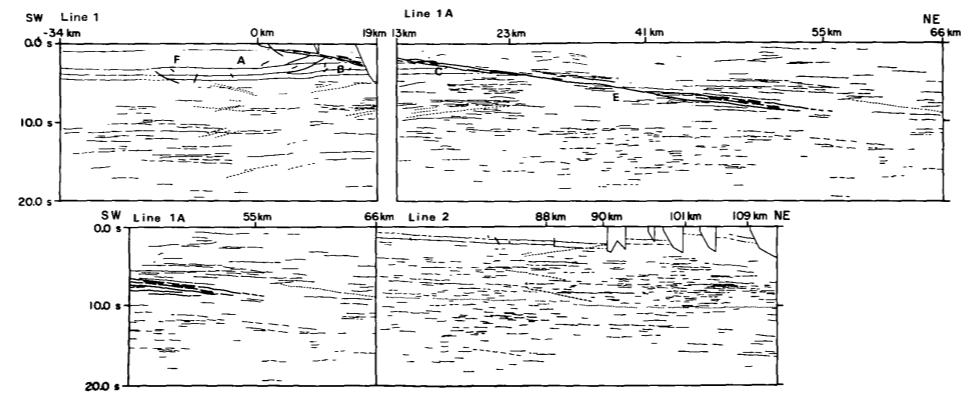
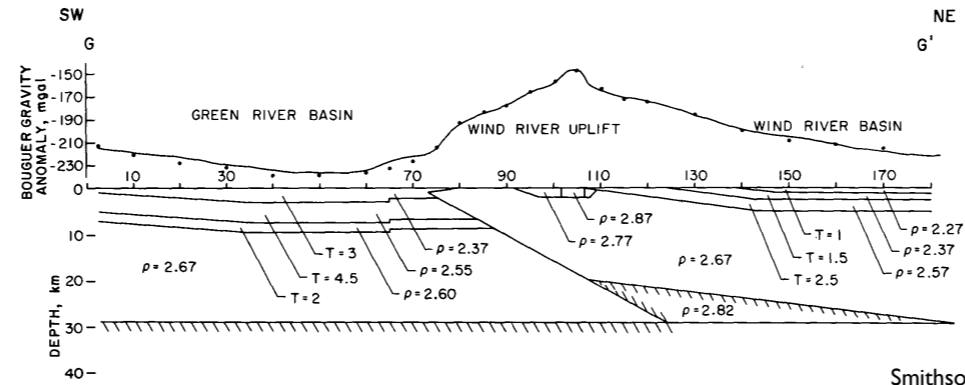


Figure 4. Interpretation of events seen on all three COCORP profiles. There is an overlap from the top northeast to bottom southwest parts of the diagram. The position of the Wind River thrust at the surface is represented by 0 km. The profiles were recorded to 20-s two-way traveltime. Dashed events represent diffractions or off-line reflections. A = reflections from flat-lying sediments of the Green River Basin. B = uplift (in time sections) of sediments underlying the Precambrian thrust over them by the Wind River thrust. C = termination of sedimentary layers against thrust with no evidence of overturning. E = appearance of thrust in the Precambrian crystalline rocks of the crust. Dotted lines represent enigmatic low-frequency event.



Smithson et al., Geology, 1978

Figure 5. Bouguer gravity anomalies and calculated model. Horizontal and vertical scale in kilometres. T = thickness of layers in kilometres;  $\rho$  = density in  $\text{g/cm}^3$ . Continuous line represents observed gravity. Dots represent modeled gravity.

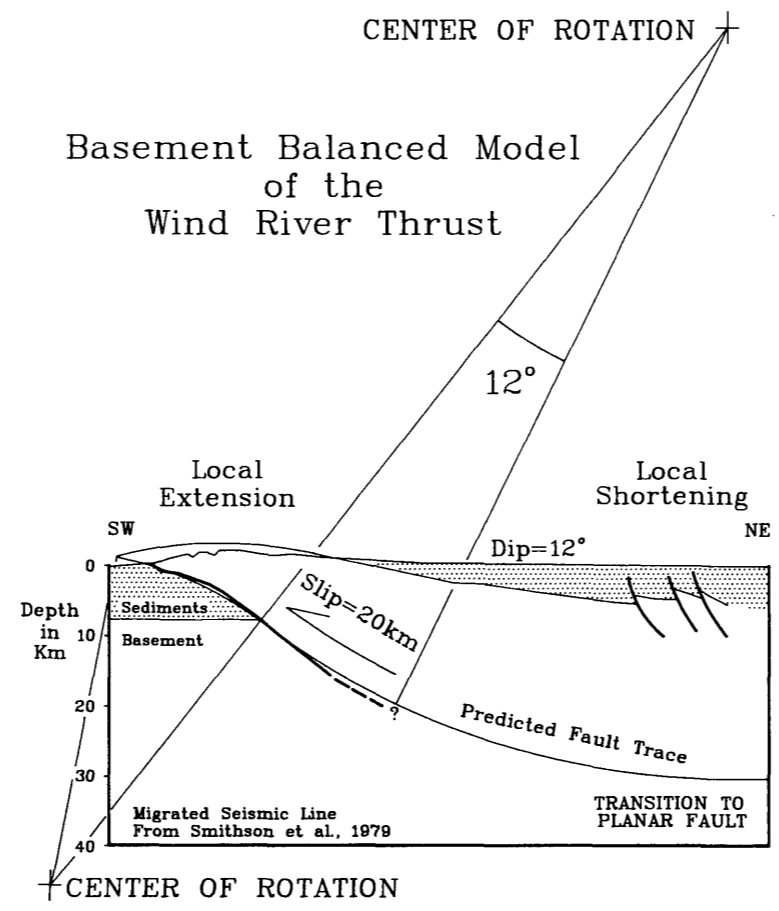


Figure 4. Illustration of congruency between seismic reflection data on Wind River thrust, Wyoming, and structural modeling discussed in text.

Erslev, Geology, 1986

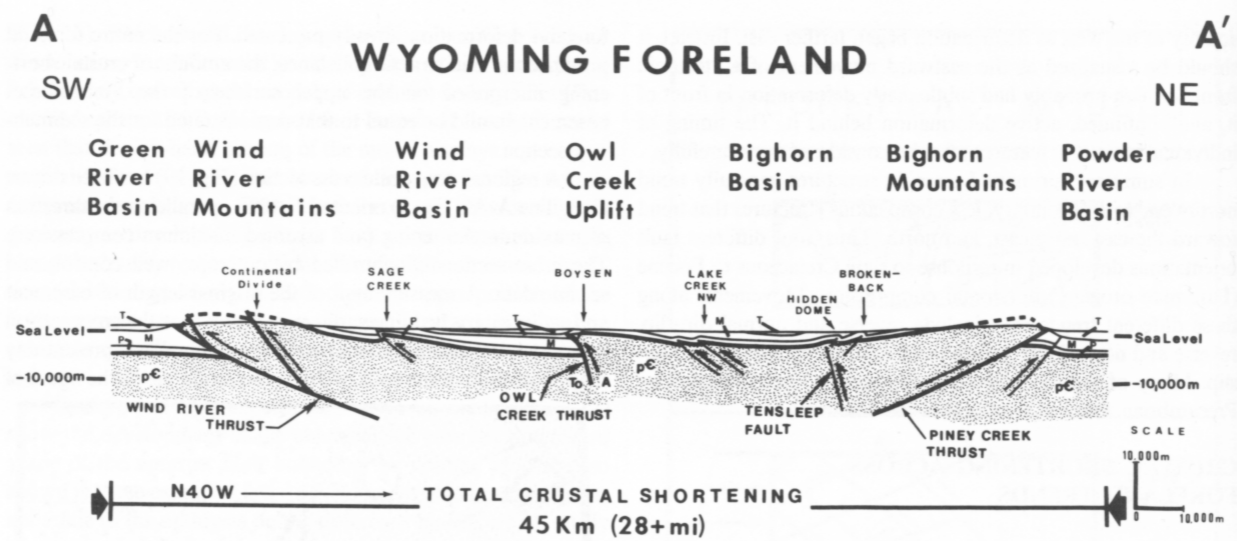
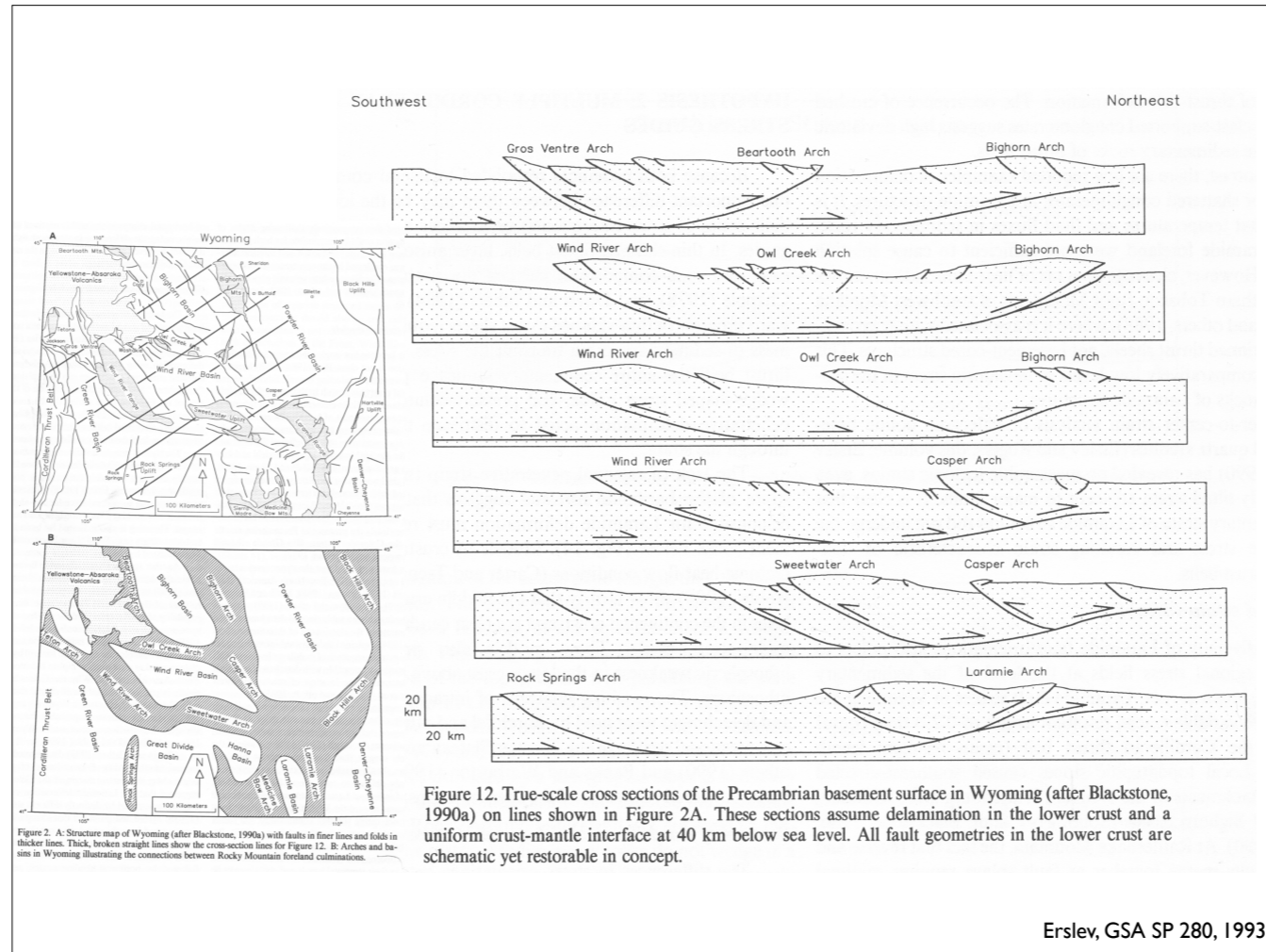


Figure 19. Regional true-scale structural cross section (line A-A', Fig. 1) drawn parallel to direction of shortening and assumed direction of maximum compression (N.40°E.), demonstrates the conjugate nature of major foreland crustal faults. Different strike orientations of foreland structures result in differing amounts of crustal shortening, as shown by crossing the east-west-trending Owl Creek thrust and Tensleep fault, as compared to the northwest-trending Wind River thrust and the Piney Creek thrust in the Bighorn Mountains. Total crustal shortening along this line of section is 45 km (about 28 mi). T = Tertiary; M = Mesozoic; P = Paleozoic; pC = Precambrian basement complex; To = toward; A = away.

Brown, GSA Mem 171, 1988

Other shortening estimates: 60-120 km by Chapin and Cather (1983) to NNE  
 43-52 km to ENE (Bird, 1998)



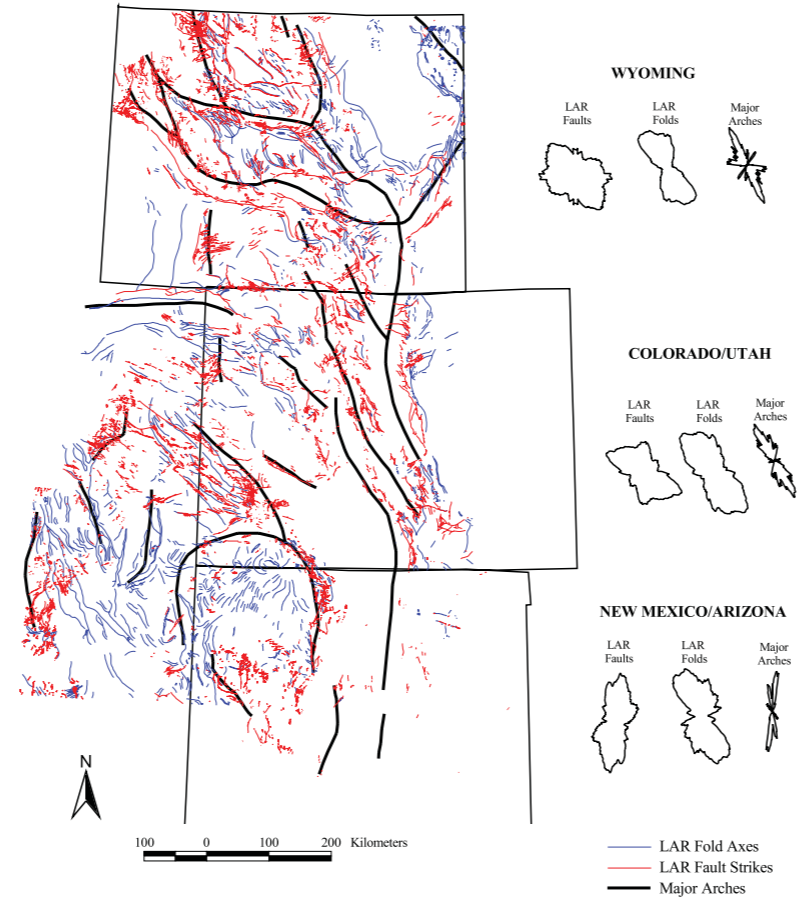


Figure 5. Map and rose diagrams of LAR arches, faults, and folds in Wyoming, Colorado-Utah, and New Mexico-Arizona.

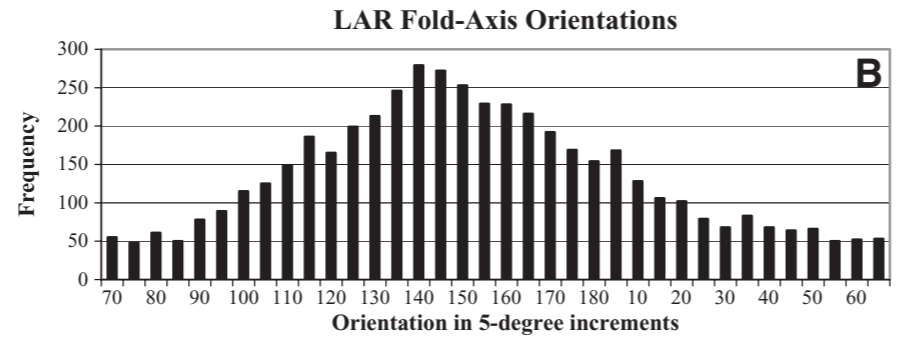
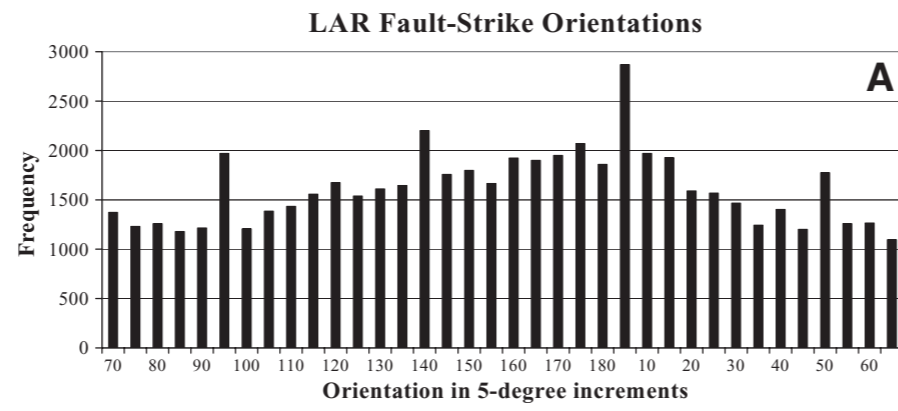


Figure 9. Histograms for all digitized LAR faults and folds from 0° to 180° in 5° increments.