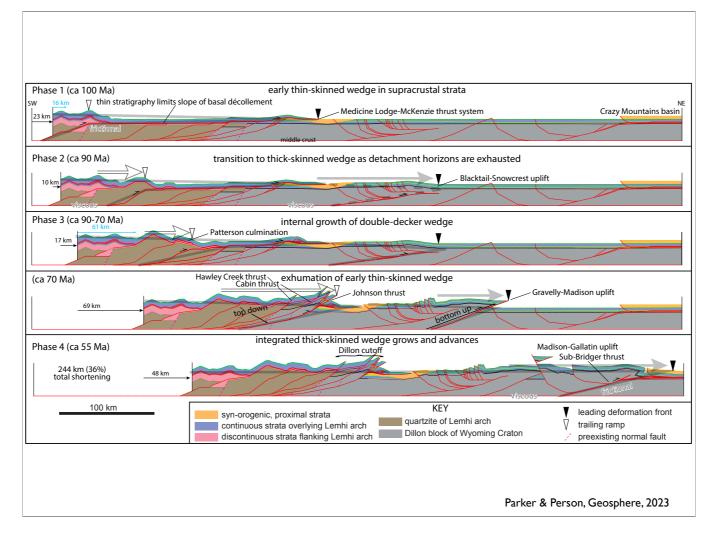
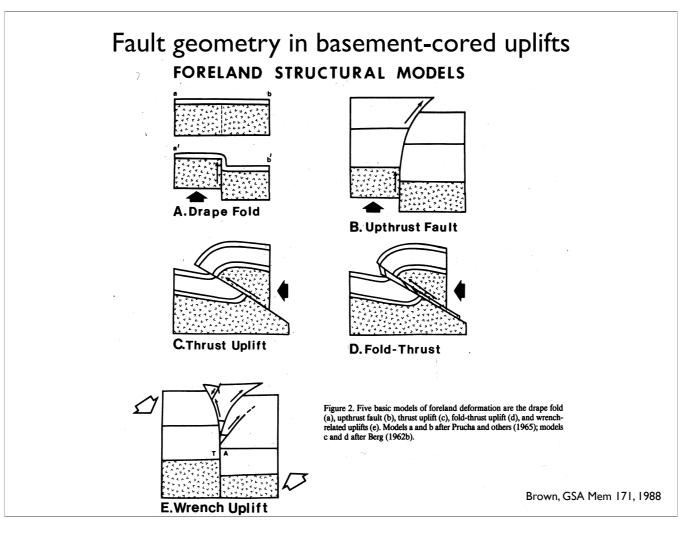


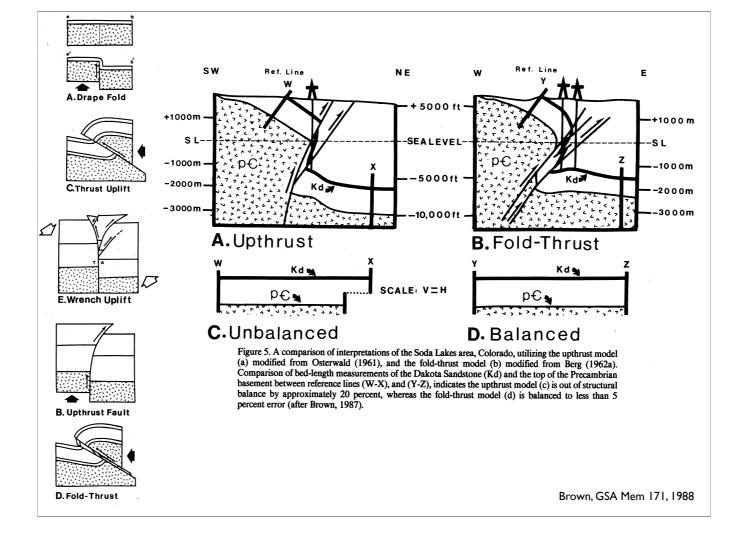
So we'll transition from the Sevier to the Laramide. Consider what these faults do at depth—what is the basis for this. Note difference in thickness of the units on thrusts to west vs foreland to east.

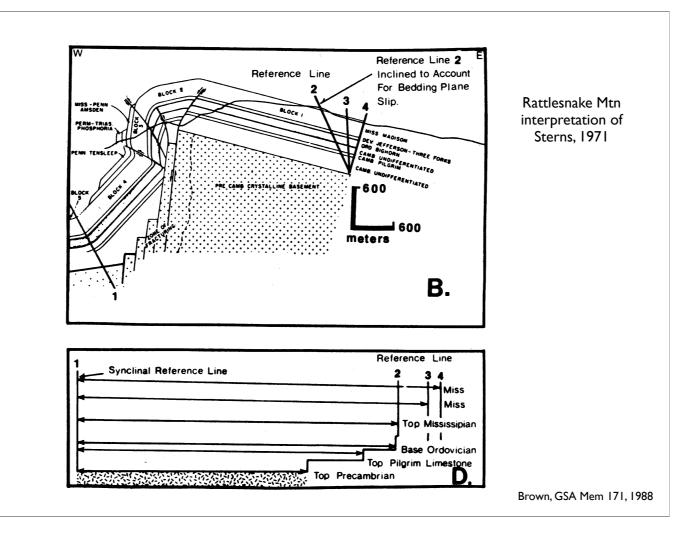


Idaho-Wyoming-Montana area where Sevier and Laramide coincide.

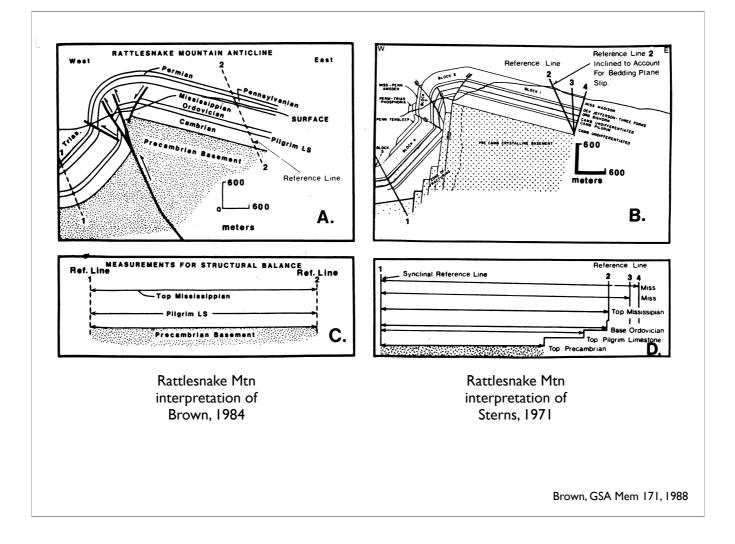


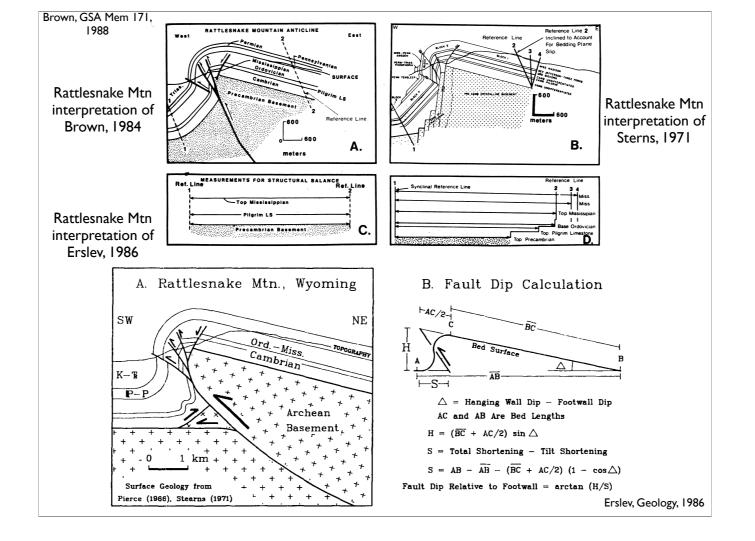
Well, as a prelude to the Laramide, let's discuss a different flavor of this: basement cored folds.

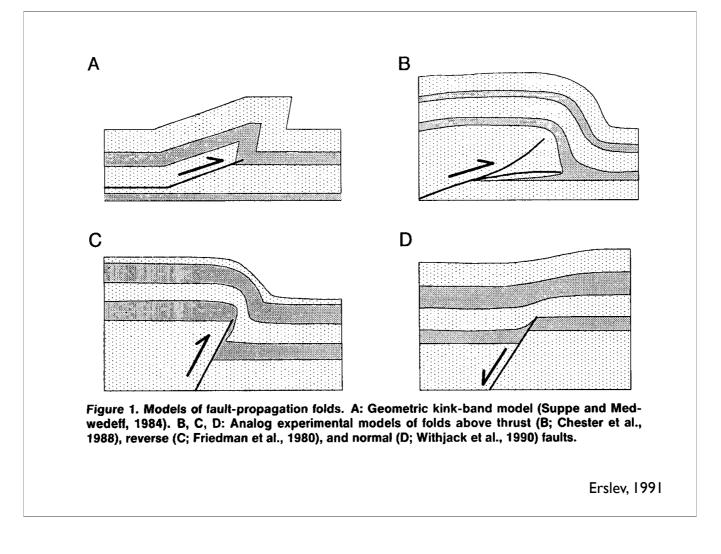


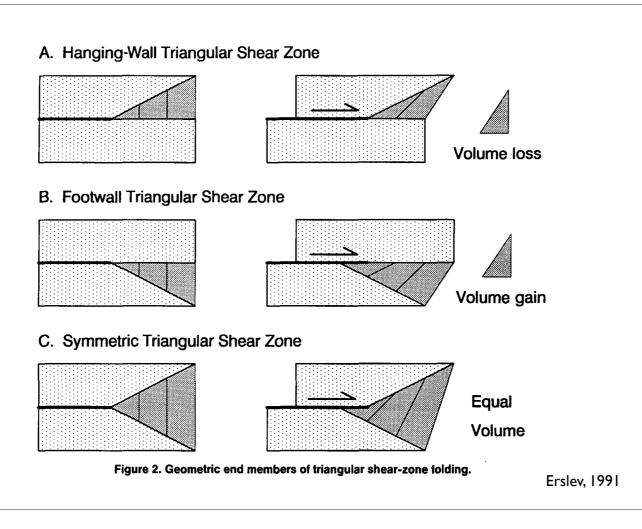


Problems with high-angle (near vertical) faulting to make these uplifts: cannot balance line lengths.

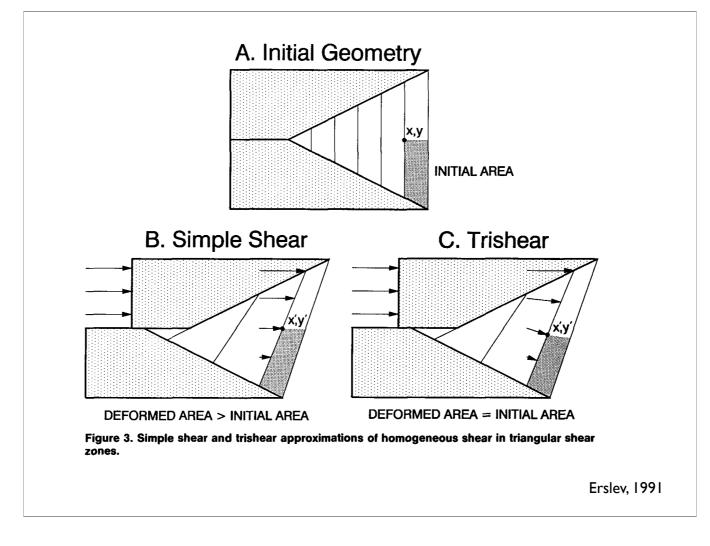


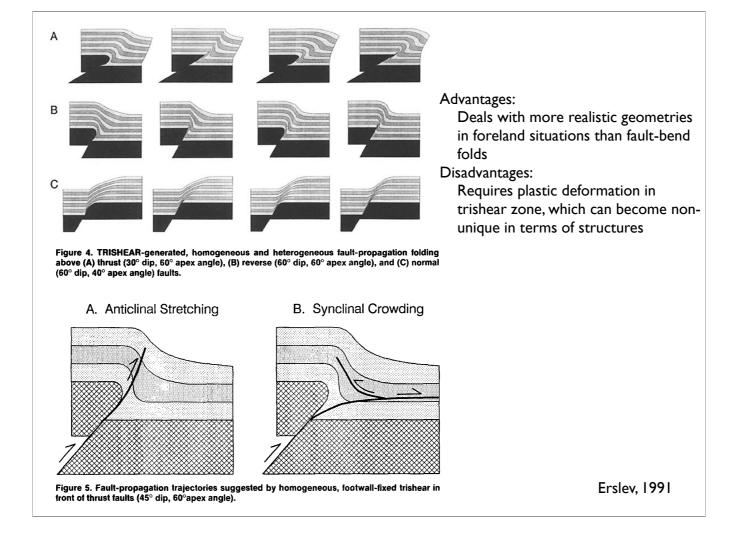


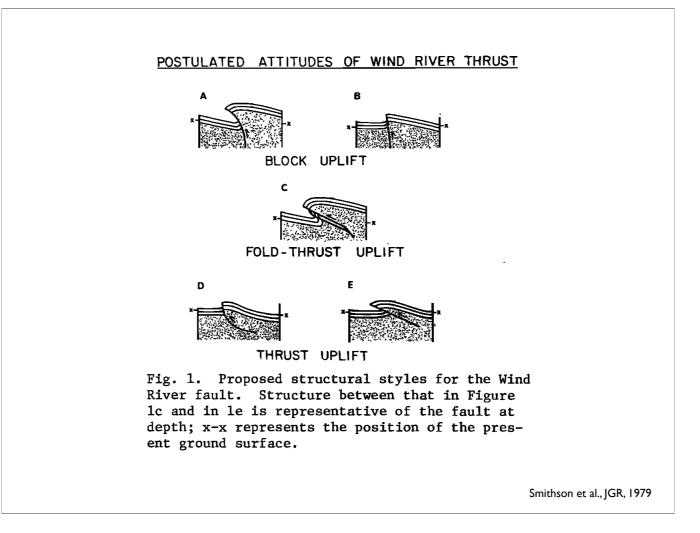




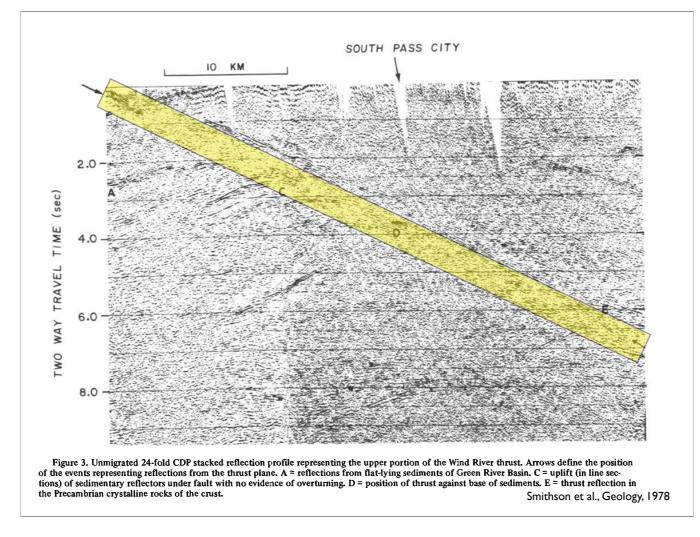
With the deformation in the trishear, this style of reconstruction conserves area but not necessarily line lengths in the plastically deforming zone.



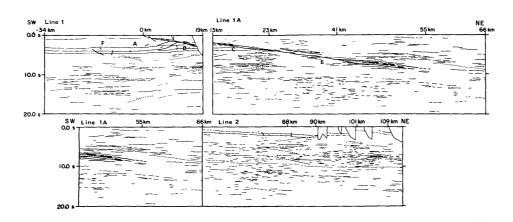


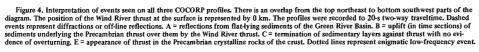


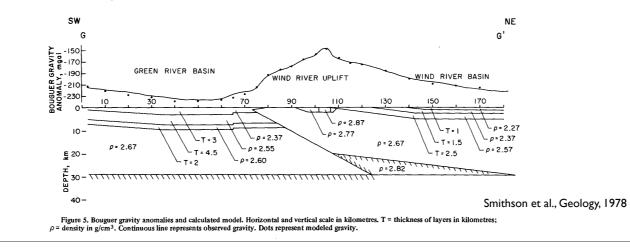
Another approach helped to kill off the block uplift models—seismic reflection profiling.

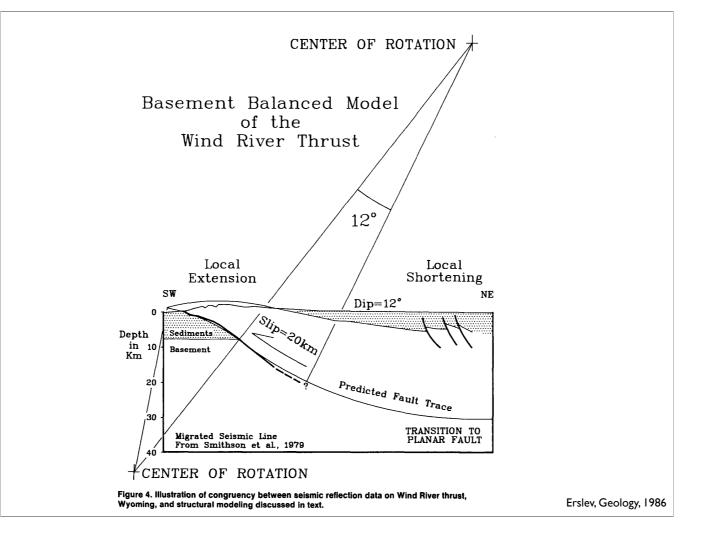


COCORP line across Wind Rivers pretty thoroughly showed that the steep vertical faults were not present, instead dipping thrust faults.

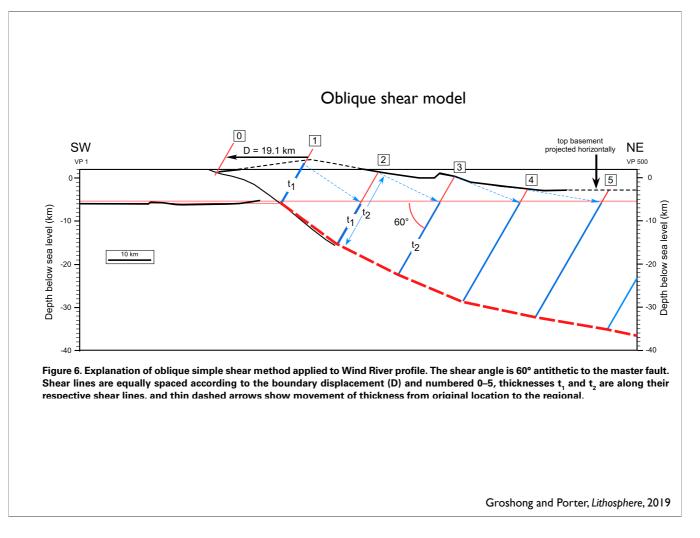




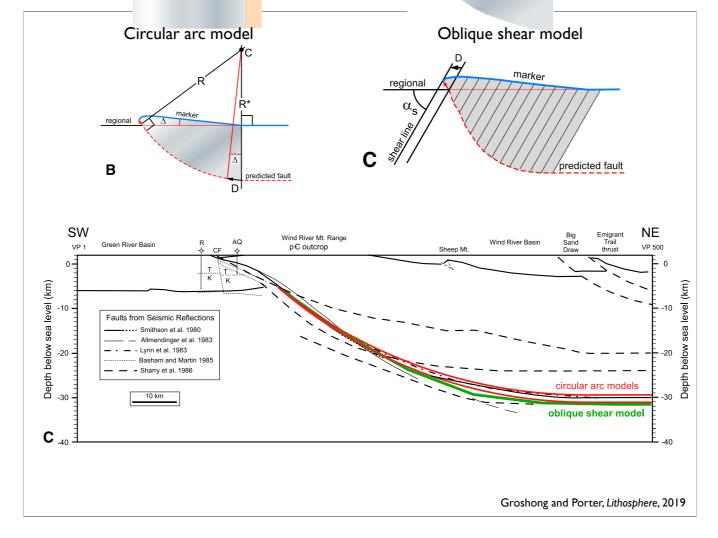




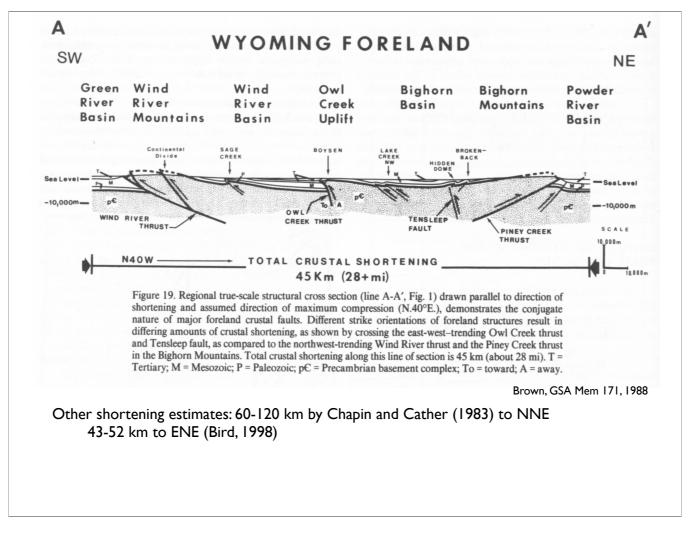
Dip on backside of Wind Rivers demands some curvature on the fault...



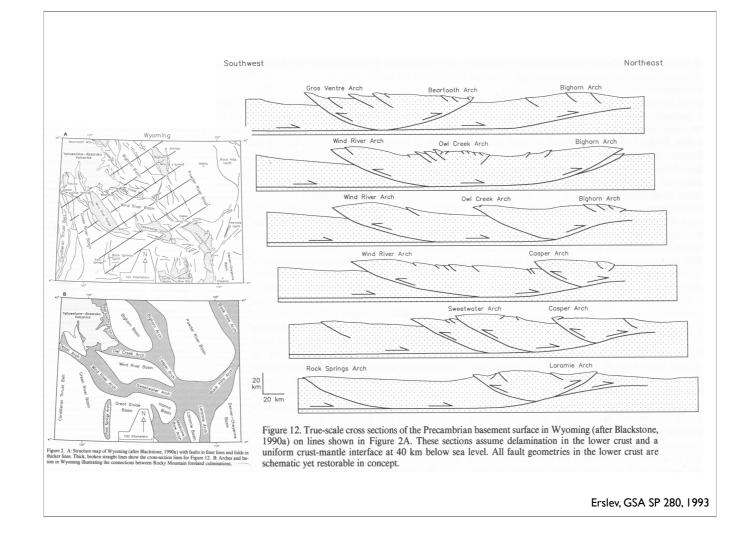
The construction of the master fault is explained here in the context of the Wind River thrust (Fig. 6). Shear lines 0 and 1 are drawn through the hangingwall and footwall cutoffs of the master fault. The boundary displacement of the block (D) is the distance between these lines measured parallel to the regional. A set of shear lines is then constructed with spacing D. Line lengths between the marker horizon and the fault are measured, starting with t1, which is restored to its original position with the top at the regional on shear line 2. The base of t1 marks the location of the fault. Then t2 is measured, shifted to shear line 3 and the fault location marked at its base. This process is continued progressively across the profile to construct the complete fault. The shear lines can be as closely spaced as desired as long as the thicknesses are always shifted to the shear line a distance D away.



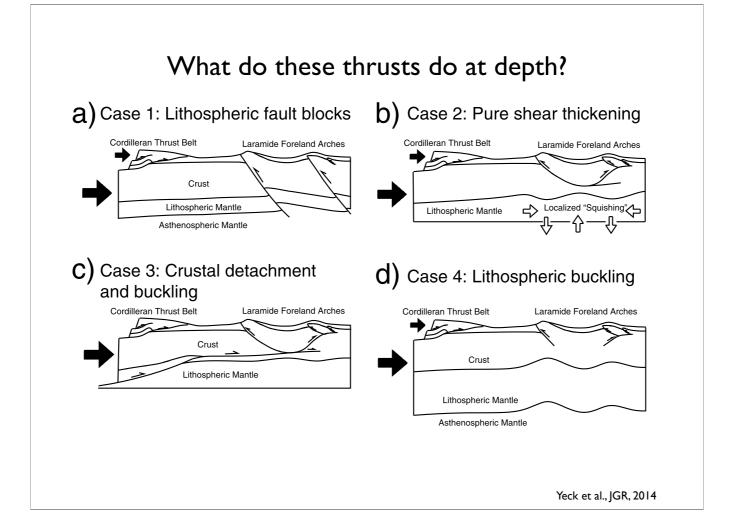
More recent analysis tends to confirm the circular arc approach (unlabeled red line is the final model determined in this paper). Note this paper puts Moho at 52 km, far below this horizontal fault. Displacements order 23 km pretty commonly inferred.

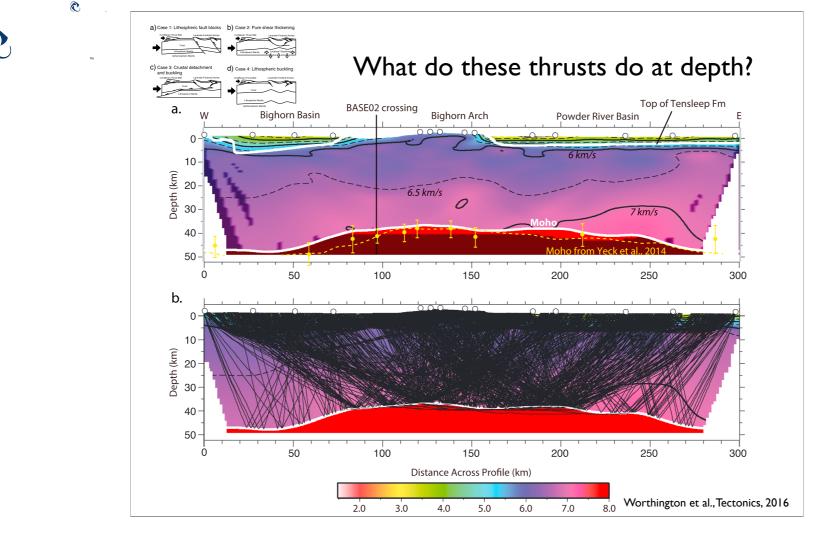


Given the Wind Rivers have 20 km themselves, 45 feels a bit short.

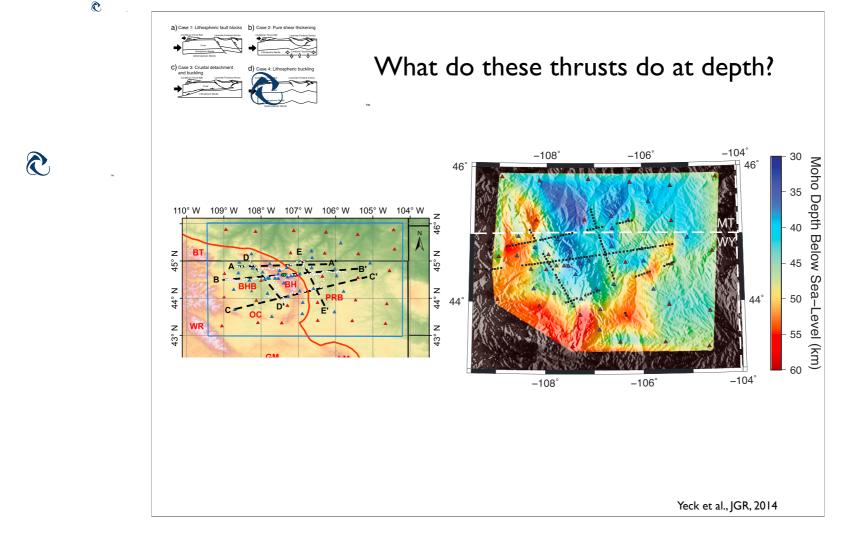




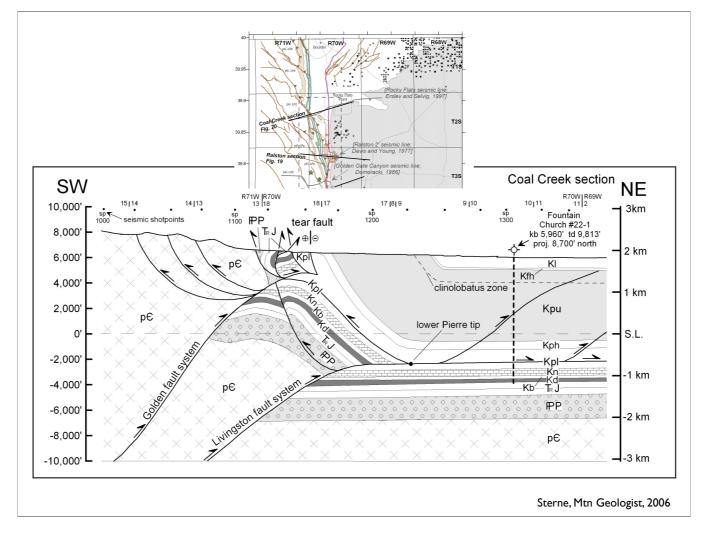




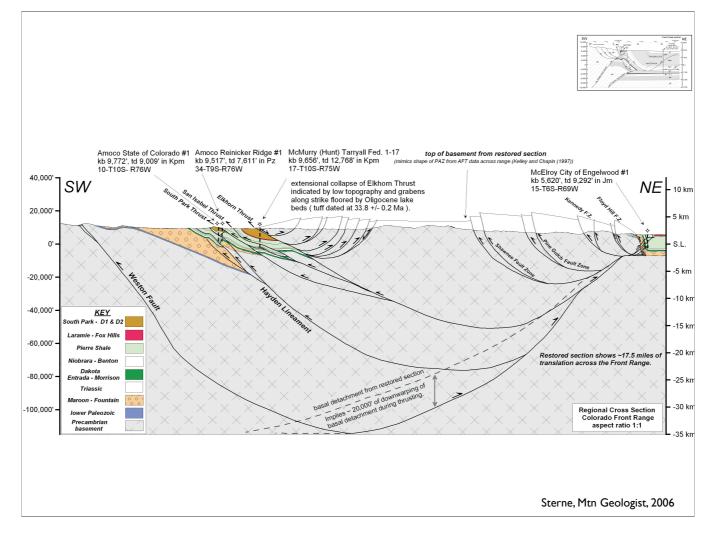
The Moho is bowed up, it seems: is this Laramide or older? Doesn't conform to any pre-experiment hypotheses. (No clear reflections from faults were ever pulled out despite considerable effort).



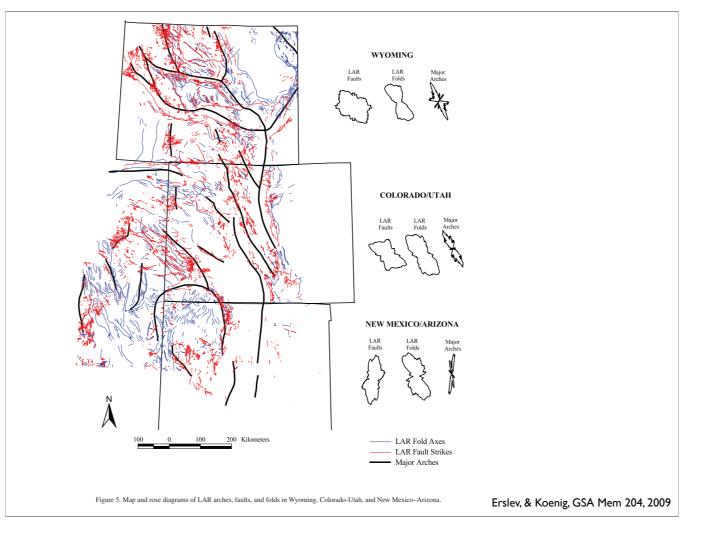
Regional estimate of Moho little better-thin under Bighorns but also to NE. Owl Creeks to south might have far deeper Moho. So...confusion?



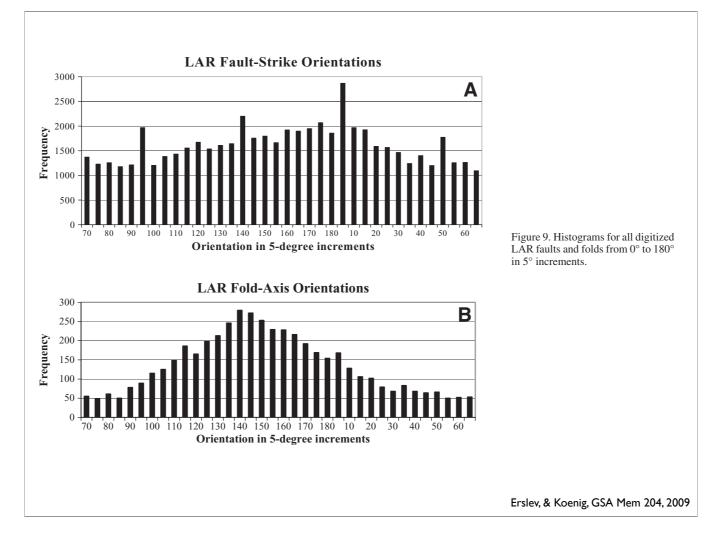
WHile the trishear models can be helpful, it seems that there are lots of complications.



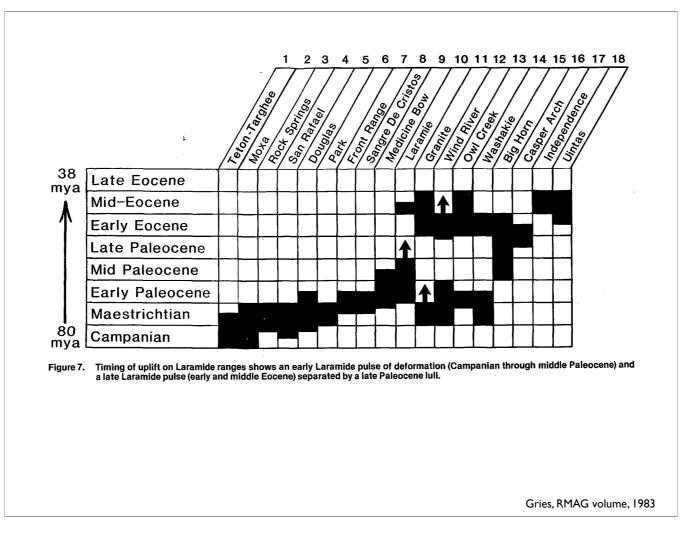
So this is a retrodeformable section in "thick-skinned" tectonics. Note the 17.5 mile (28 km) shortening across Front Range [but note, if shortening was oblique, movement was greater].



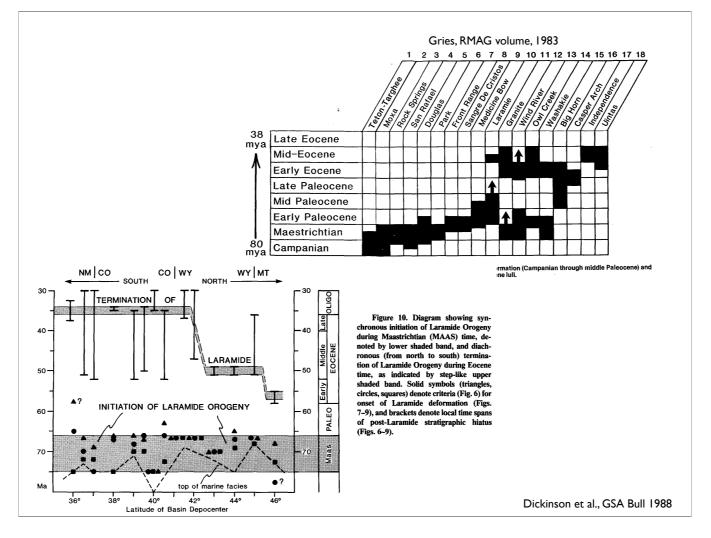
Of course, you have to balance in proper shortening direction—which might be reflected in the geometry of folds and faults.



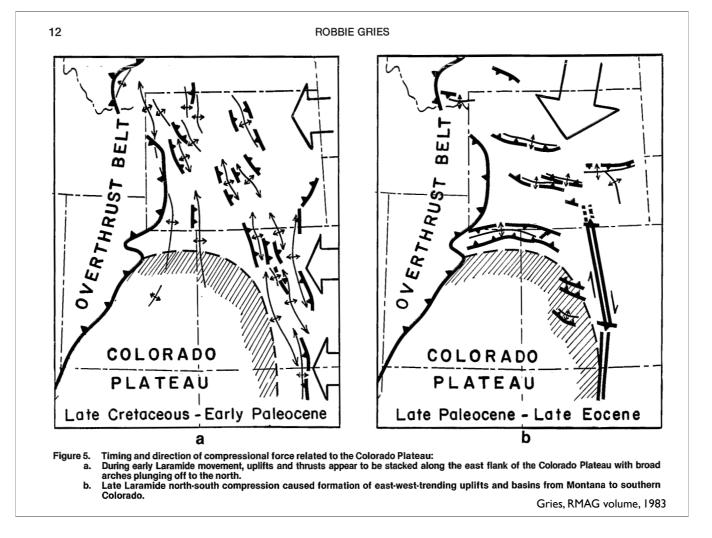
Faults, curiously, show no bias, perhaps reflecting reactivation of all sorts of older structures. But folds do cluster near 140 (S40E), suggesting a N50E shortening direction.



Yet others had inferred two episodes of deformation with different orientations [and while I think the different orientations idea is fading out, the two times of shortening seems more resilient].



There was disagreement on the timing, though...



How do we test ideas like this? After all, the ranges vary in strike. One approach is to determine the stress tensor consistent with observed deformation (an approach with a problem at its source, namely that the strain is quite finite, so stress no longer linear with strain).

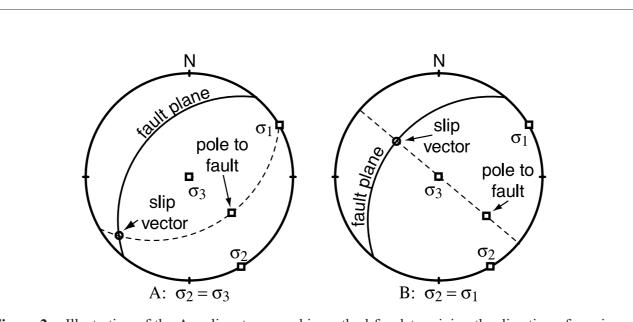
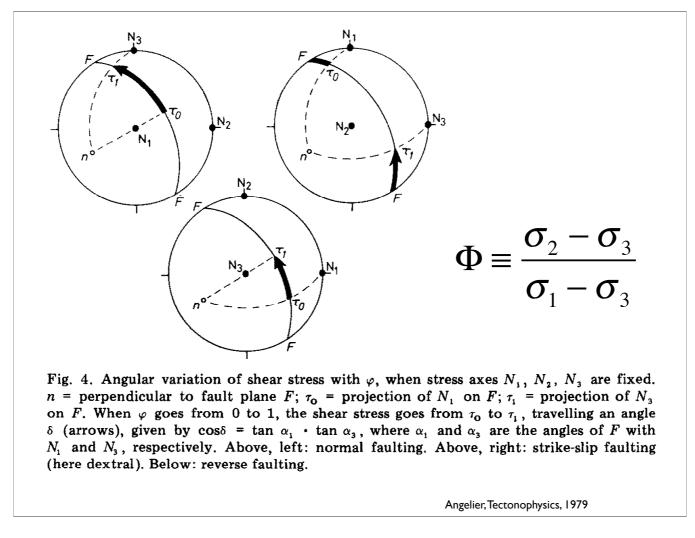
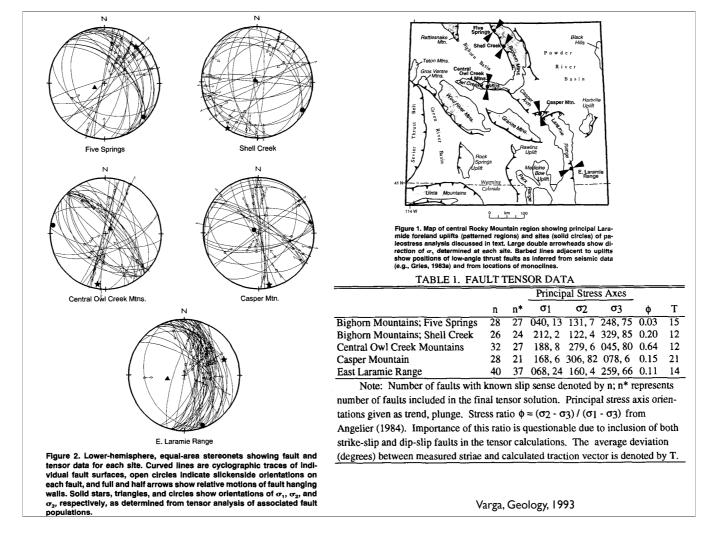


Figure 2. Illustration of the Angelier stereographic method for determining the direction of maximum resolved shear stress (and predicted slip) on a fault plane of given orientation [after *Angelier*, 1979]. Both Figures 2a and 2b are lower hemisphere projections showing the same fault plane and principal stress axes. (a) In the limit that σ_2 is equal in magnitude to σ_3 the slip vector is the line of intersection between the fault plane and the great circle that includes the pole to the fault and the σ_1 axis. (b) In the limit that σ_2 is equal in magnitude to σ_3 the slip vector of the fault plane and the great circle that includes the pole to the fault and the σ_2 values predict slip directions between these two endpoints.

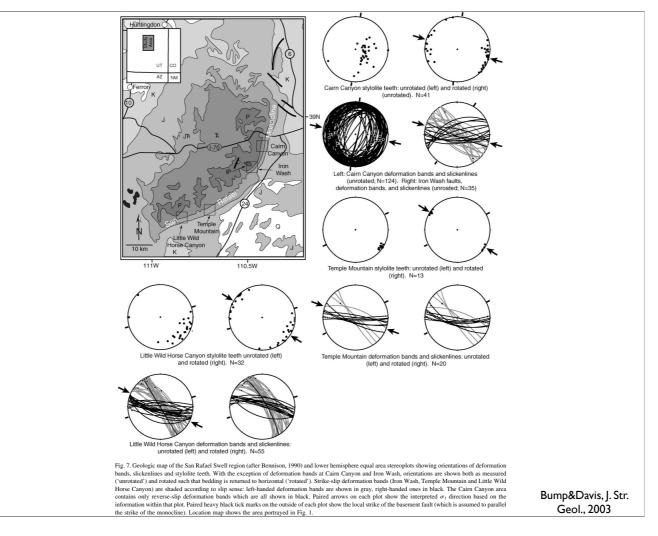
Bump, Tectonics, 2004



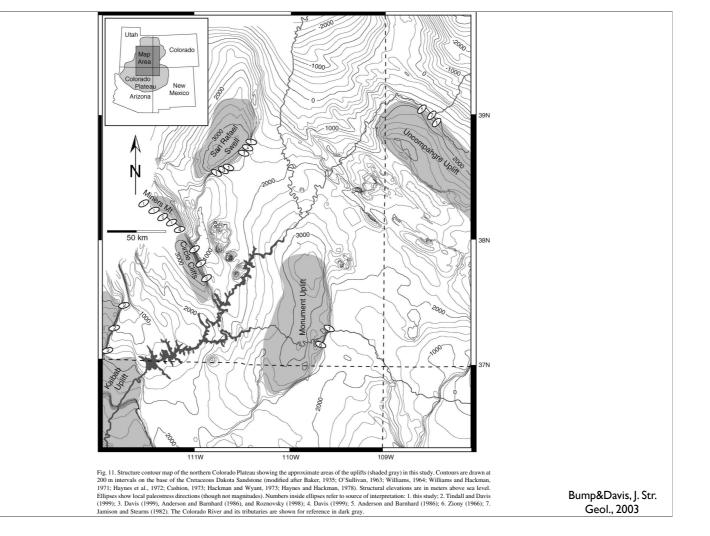
In essence, shows how slip vector on a given plane maps to values of Φ (τ_0 is where phi is 0 ($\sigma_2 = \sigma_3$), τ_1 is where phi is 1 ($\sigma_2 = \sigma_1$)



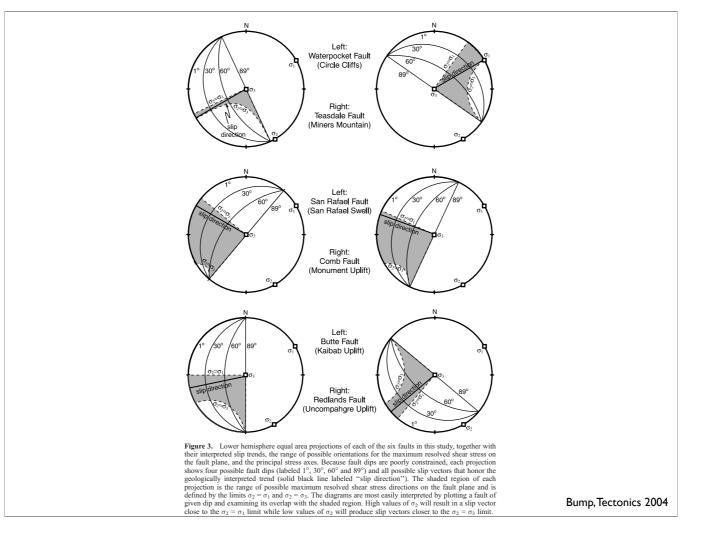
Although the data as presented suggest range-normal shortening, the author ended up preferring a slip partitioned solution.



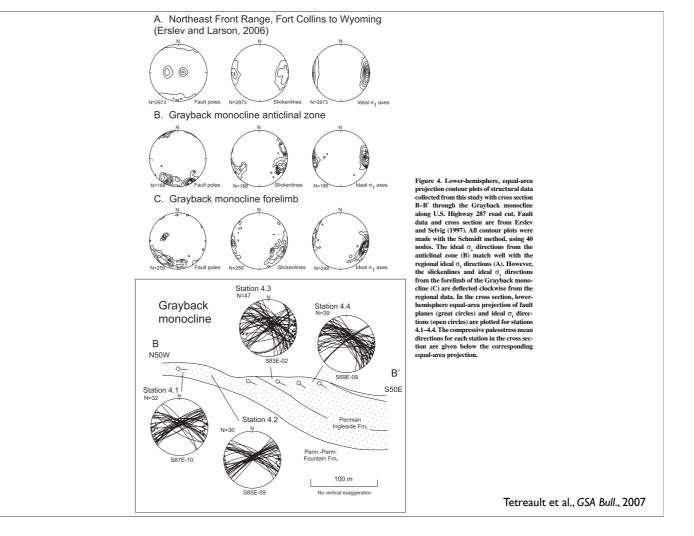
On the Colorado Plateau, get something different.



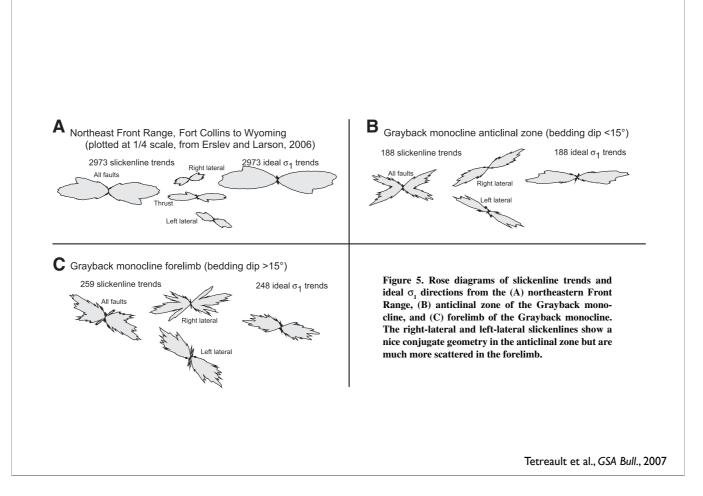
Again, varying trends of structures-does this require multiple stress fields?



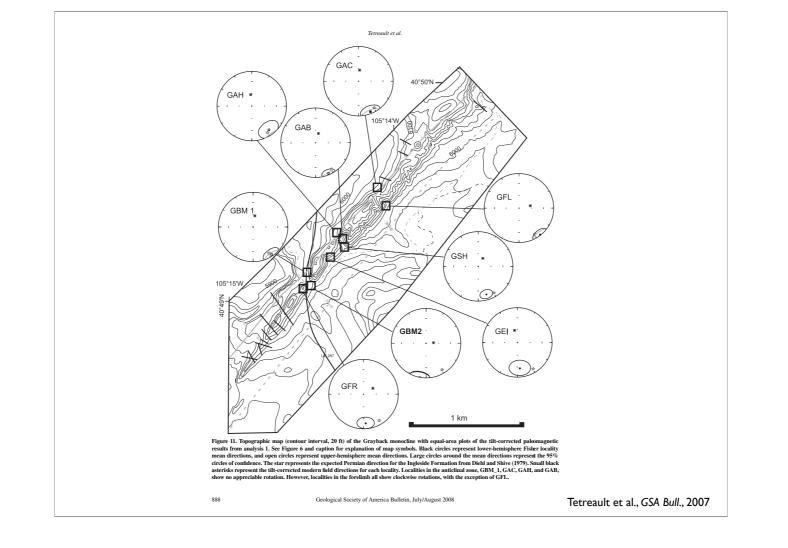
Bump seems to be suggesting that all these different slip vectors could be a single stress orientation with varying relative strength of sigma 2.

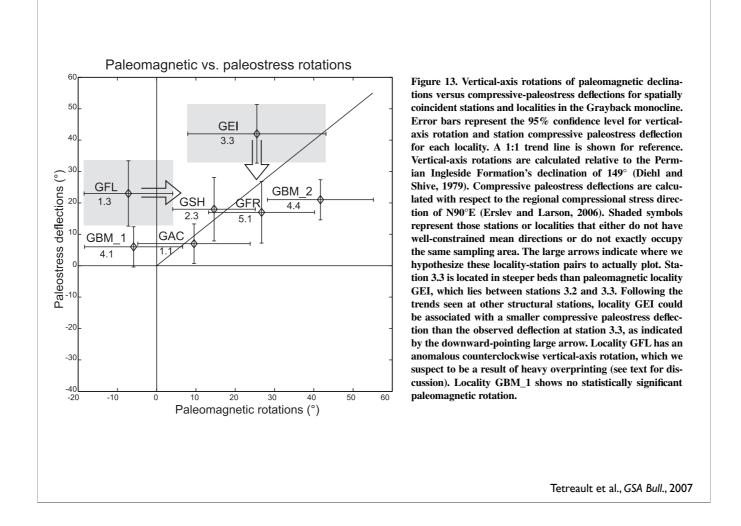


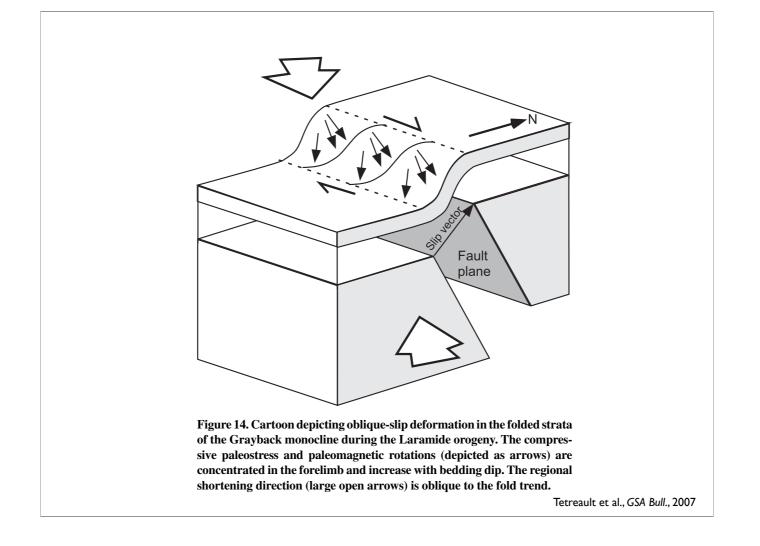
But there might be other complications out there. Perhaps more complex deformation.



Stresses in this fold depend on where in the fold you sample.



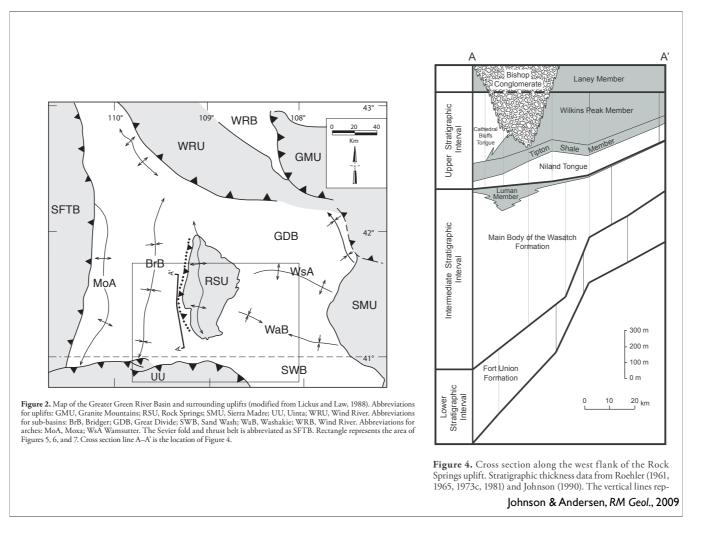




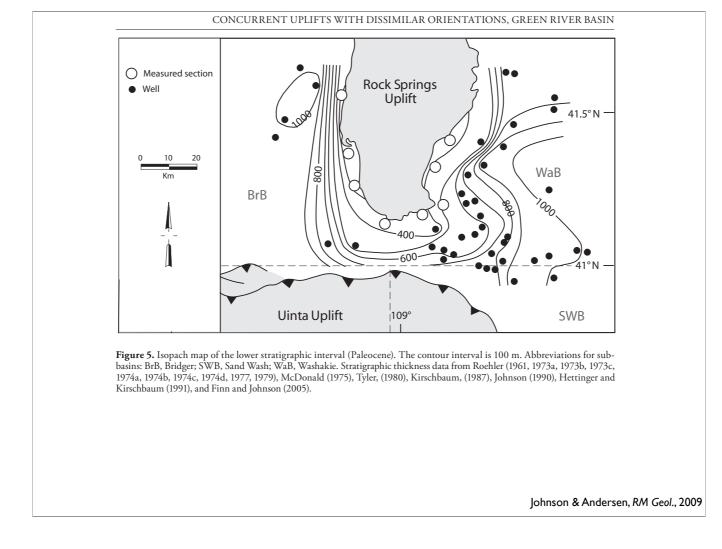
R

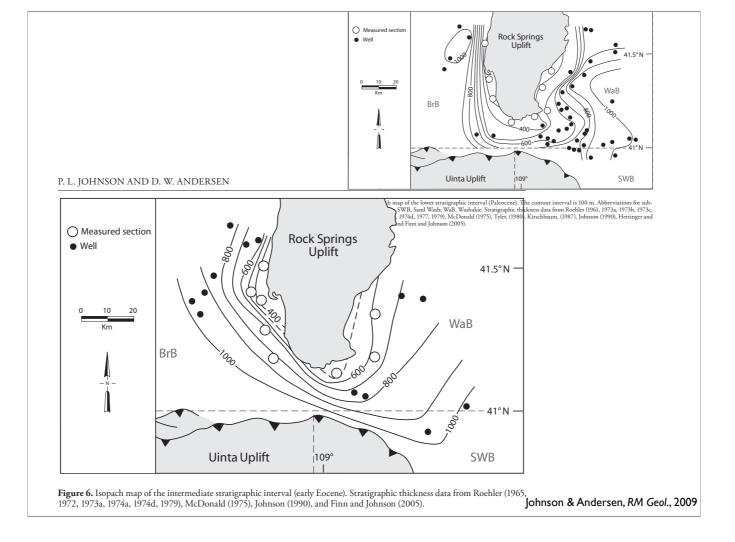
R

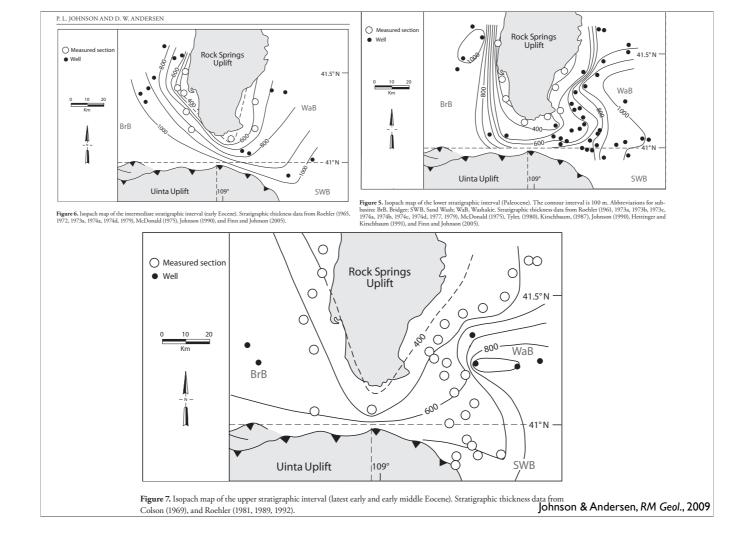
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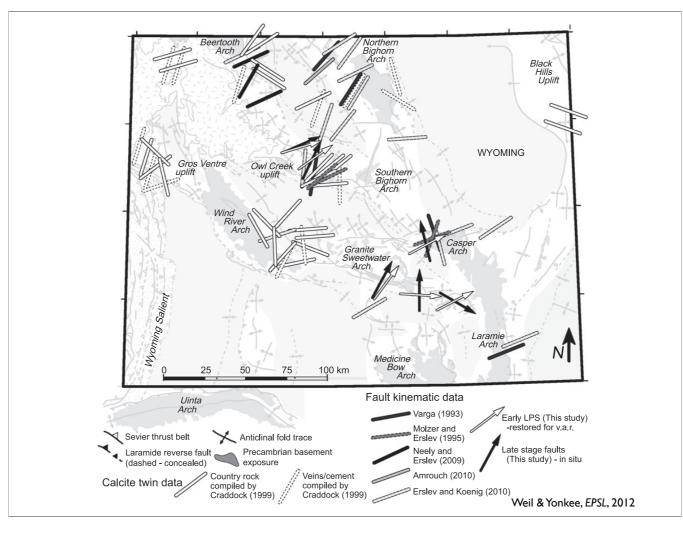


Notice presence of north-south Rock Springs uplift near east-west Uintas and folds to east. Are these synchronous?

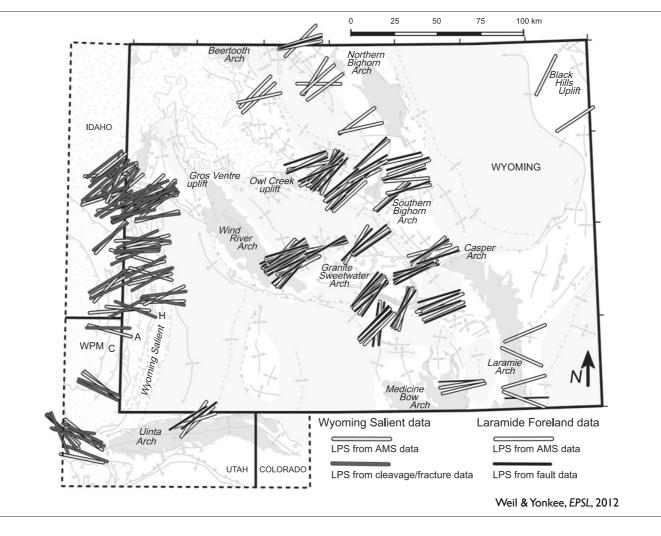




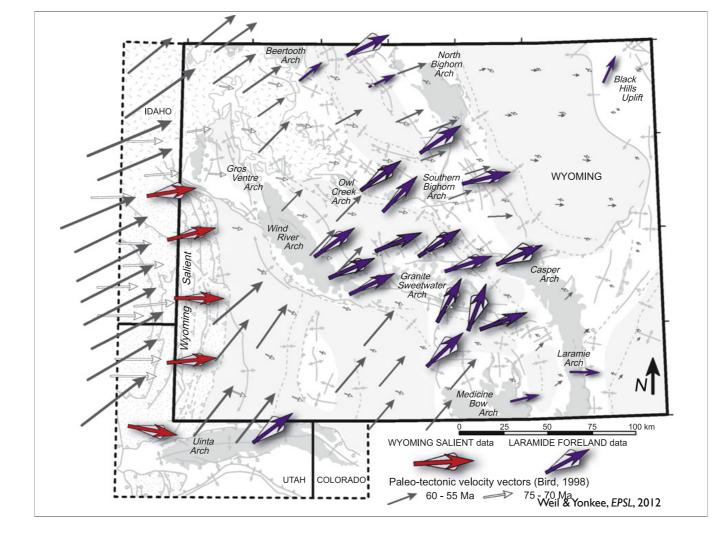


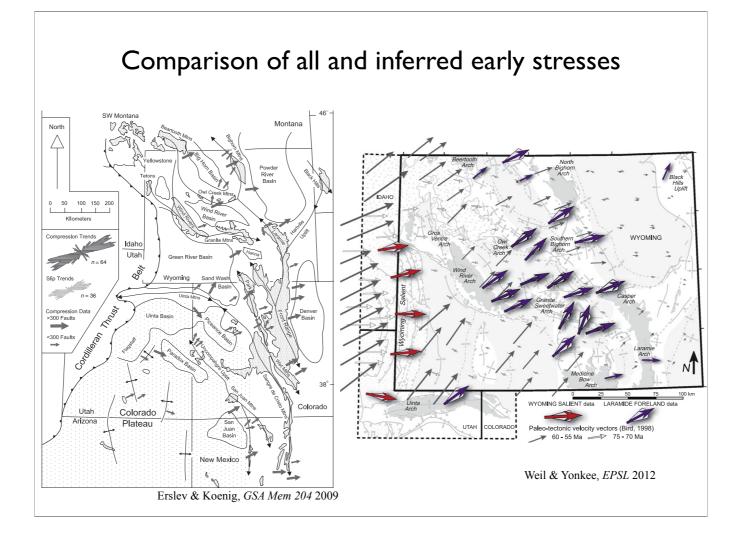


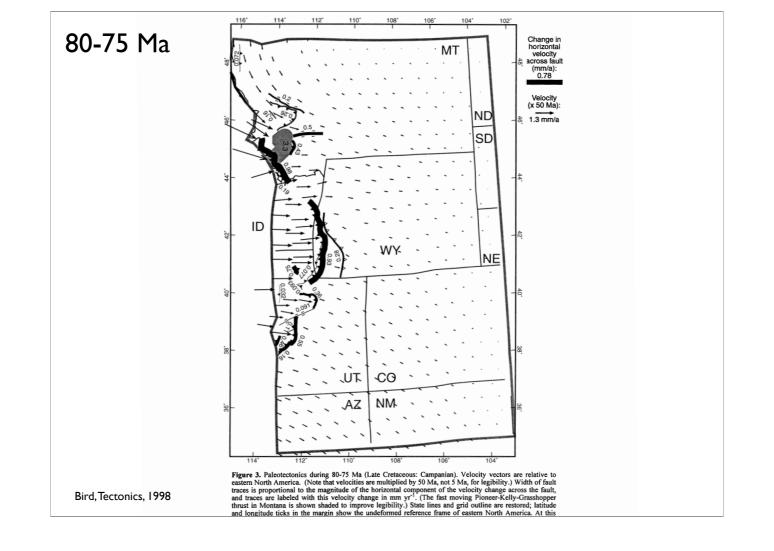
Pre-study estimates of fault kinematic data and early vs late fault slip--argue that the development of folds results in locally reoriented stresses and so these aren't robust indicators of regional shortening/stress field.

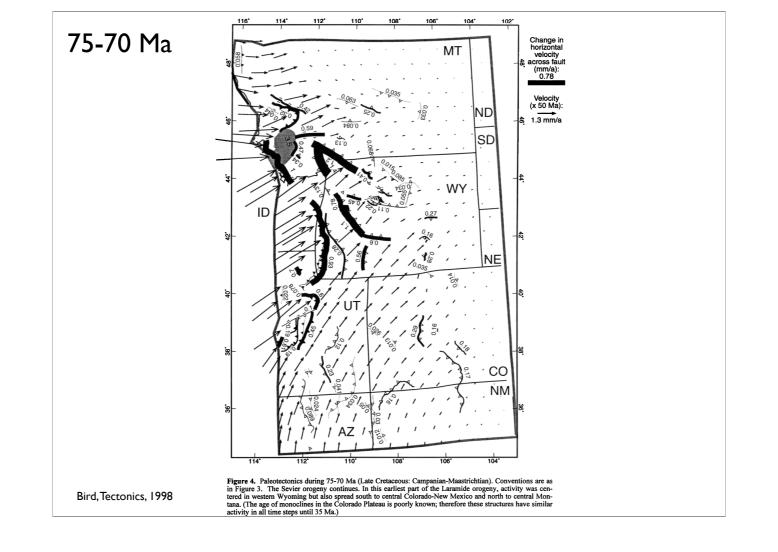


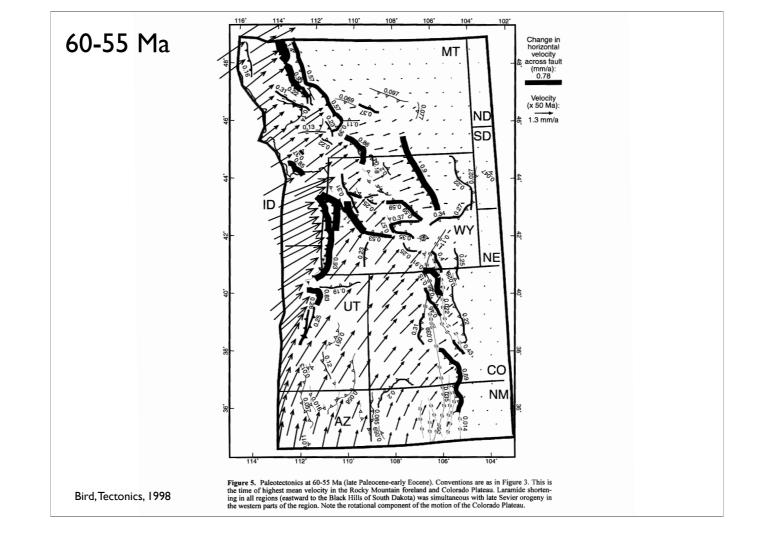
LPS is layer-parallel shortening. Stuff on the left is Sevier-style, center and right is Laramide-style

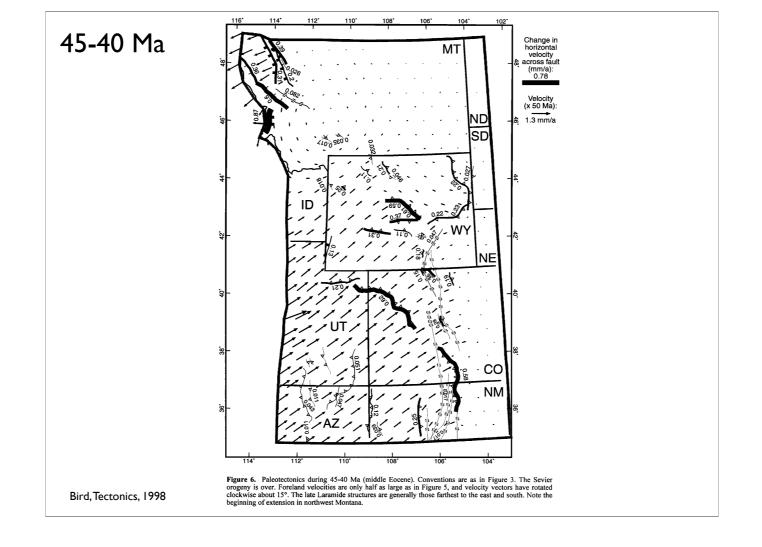


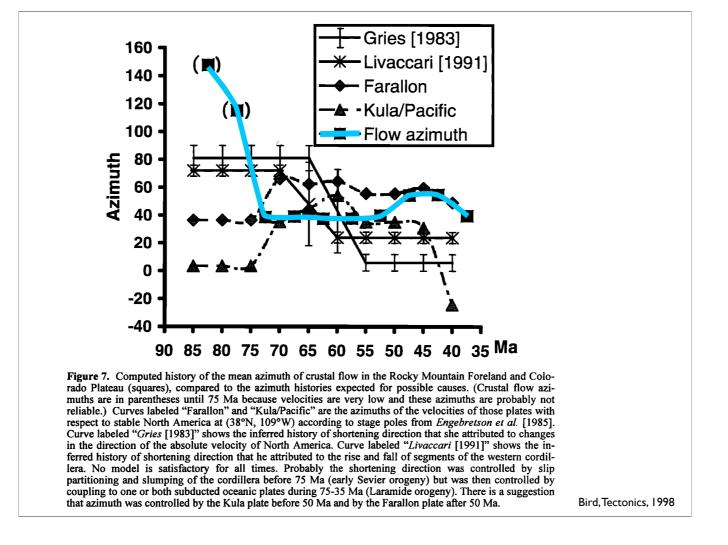












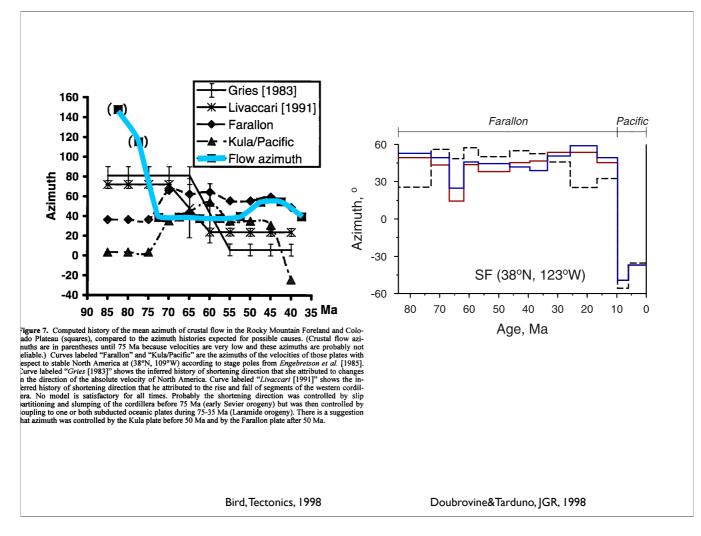
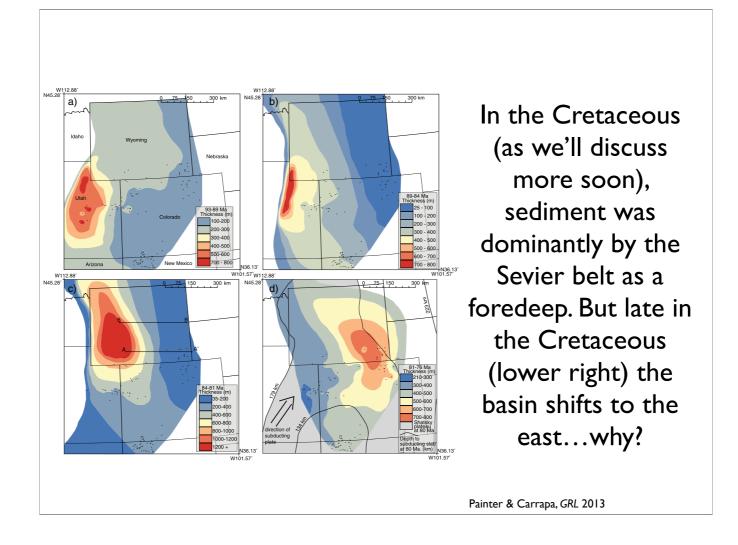
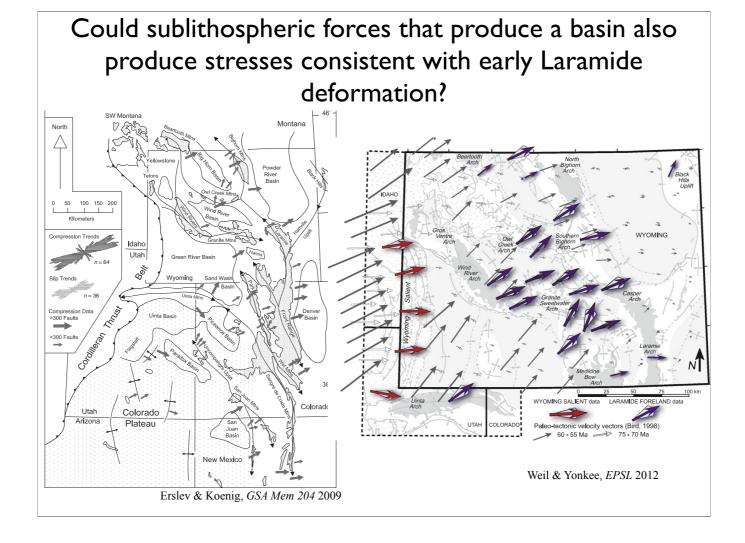


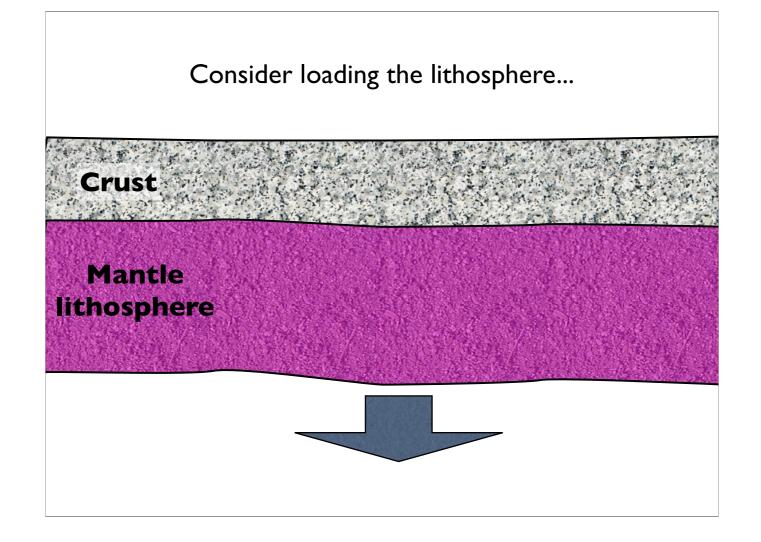
Plate circuit reconstructions tend to increase obliquity of Farallon subduction somewhat (solid lines—blue is Engebretson Far-Pac, red is Mueller Far-Pac, dashed is Engebretson fixed hotspot).

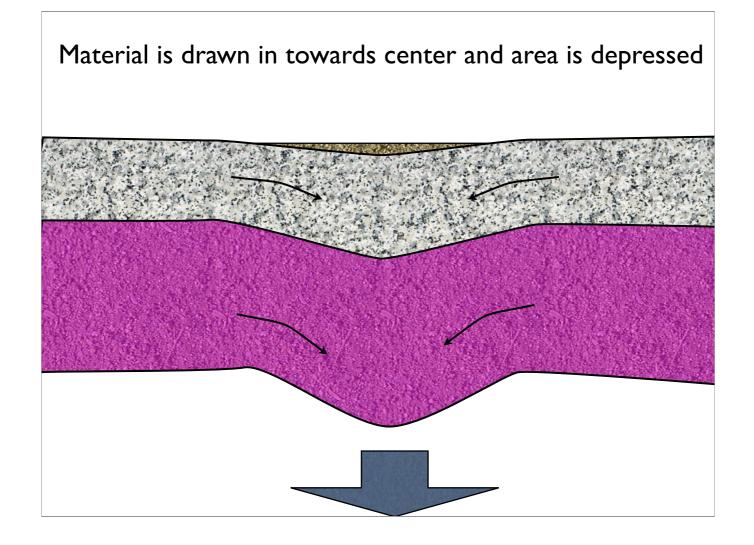
Does the parallel of Bird's shortening and the NAM-Farallon direction mean there was coupling under the continent with the slab?

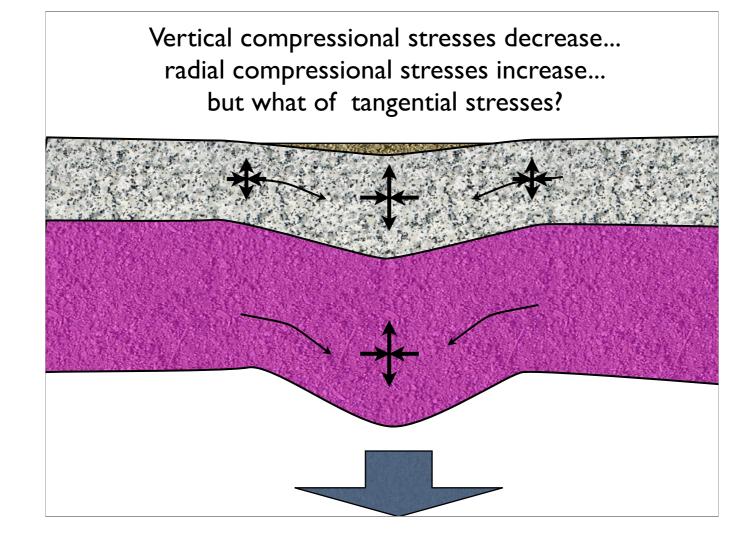
Certainly possible, but maybe another thing to look at...

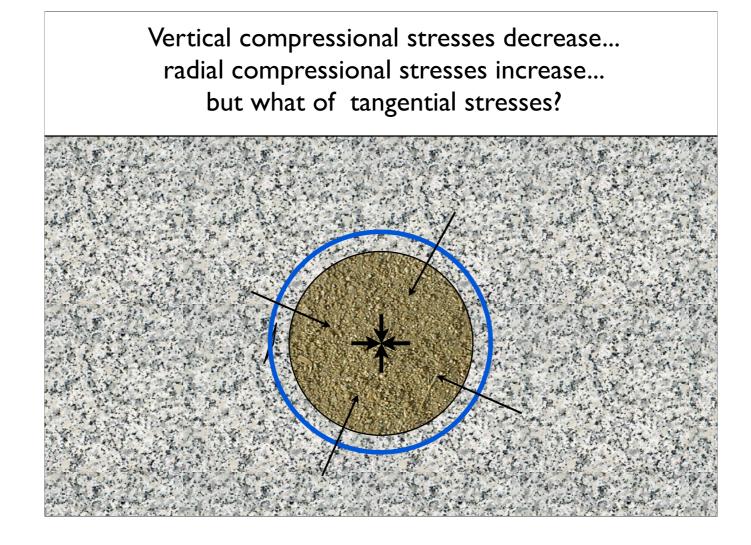


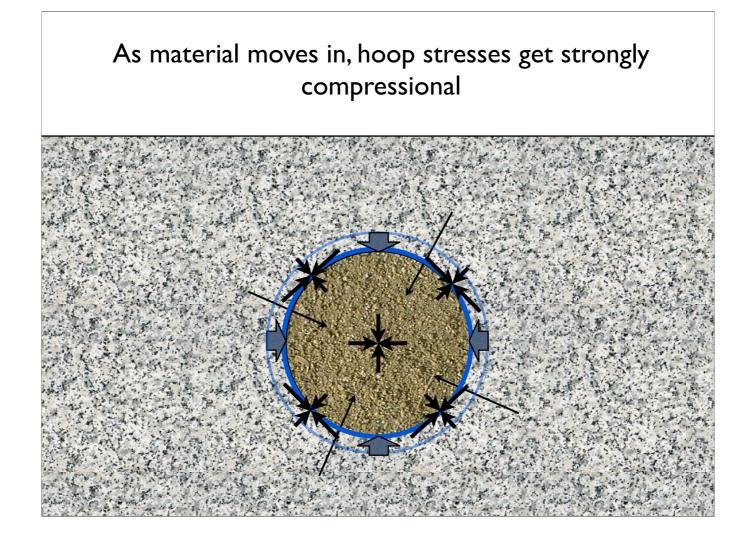




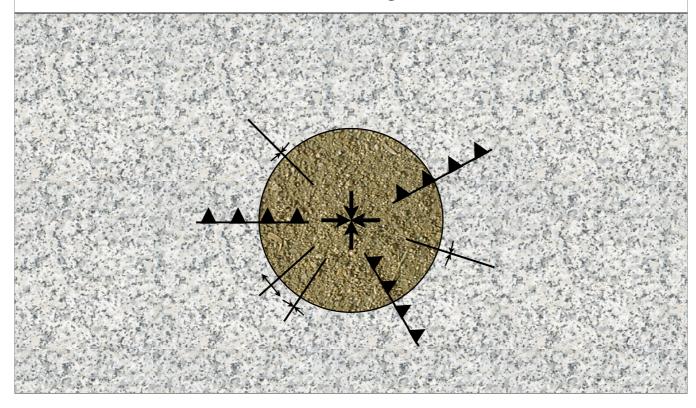


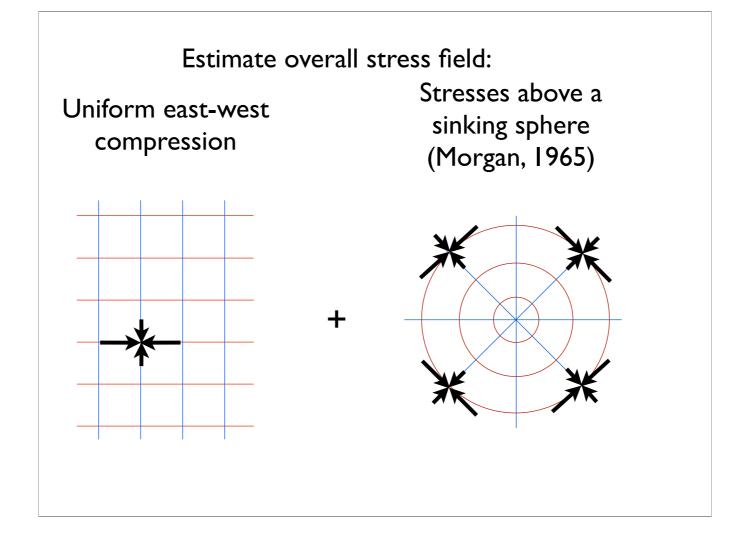


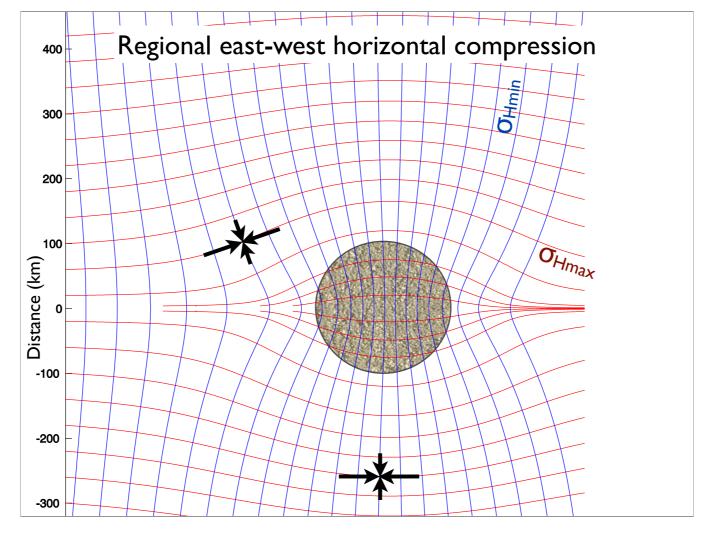




So you could expect radially symmetric folding or faulting But what if there is a regional stress field?







Exact degree of bending of stresses depends on the ratio of the load to the regional stress field.

